

Statistics Workbook

Certified Inspector Training Program



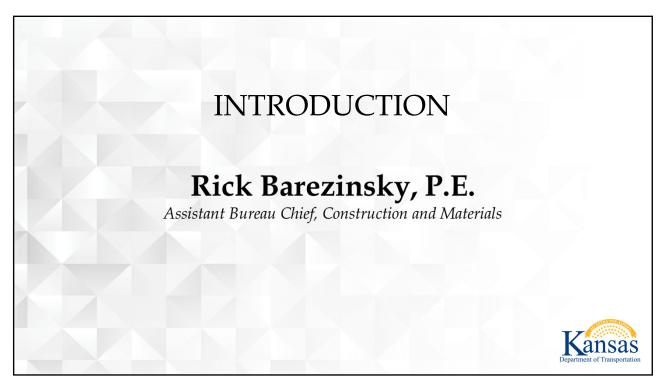
Statistics Workbook

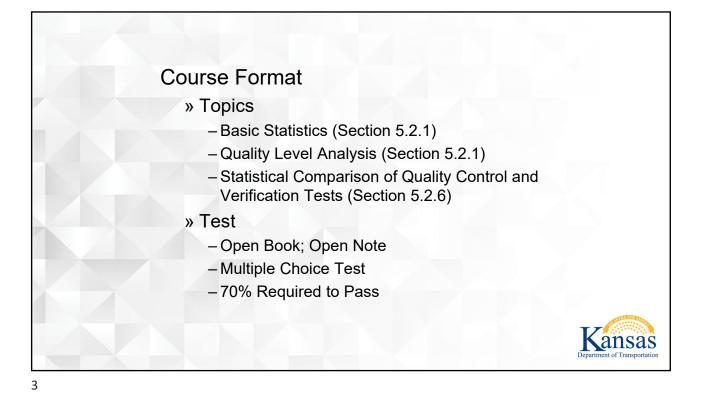
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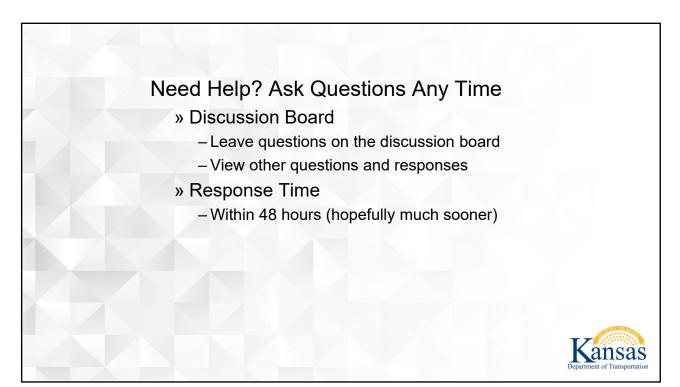
Click on the section name below to be taken to the correct page.

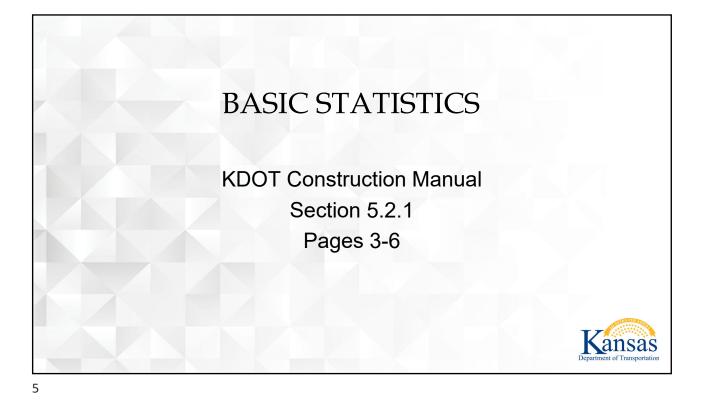
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- 2. Normal Distribution Curve
- 3. Quality Level Analysis
- 4. Statistical Comparison of Quality Control and Verification Tests
 - a. Part 1 F-test method
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- 5. Practice Problems

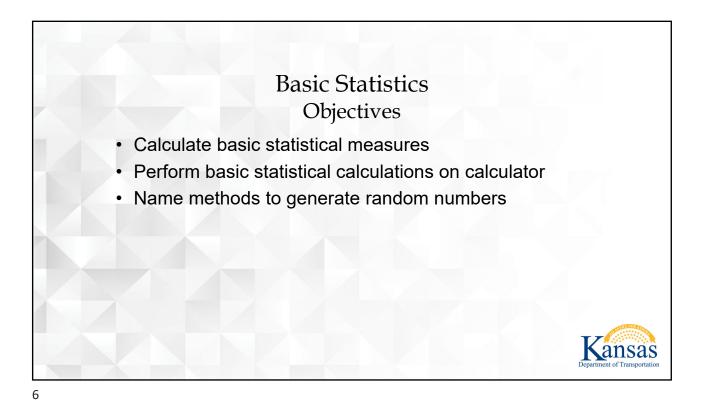


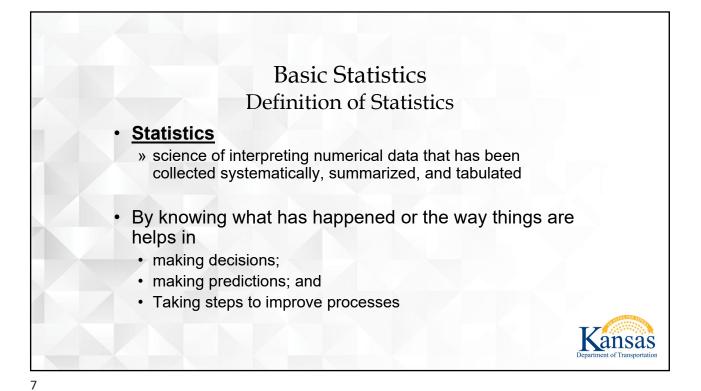


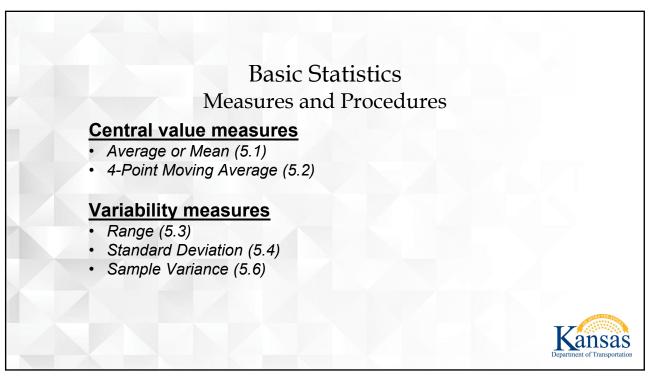












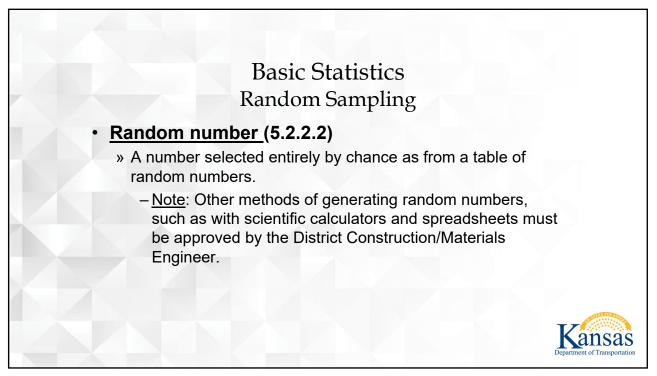
Basic Statistics Common Terms

Data Set - a group of data (numbers)

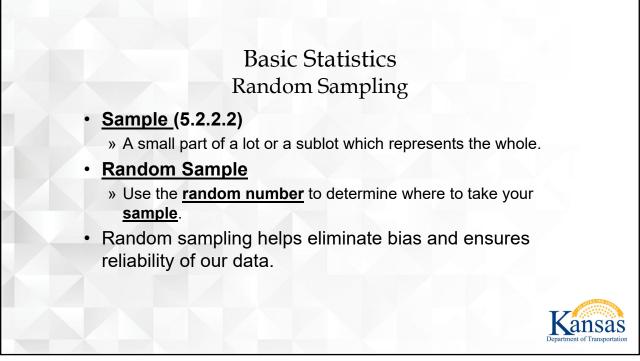
» Numbers usually represented as variable (x_i)

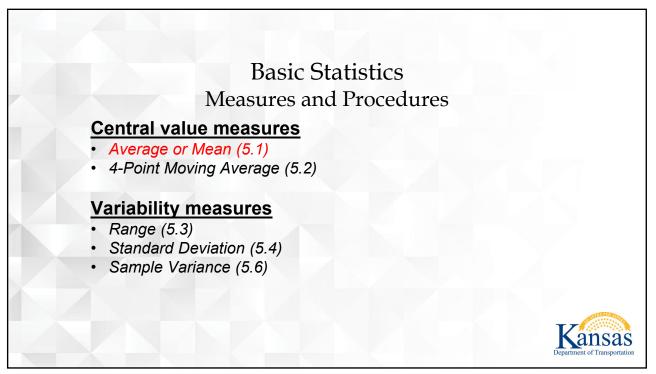
- $-x_1$ represents first number in data set,
- $-x_2$ represents second number in data set, etc...

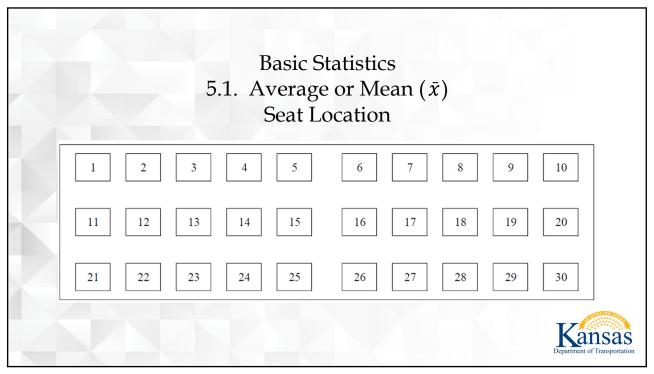
» Total number of variables represented as n



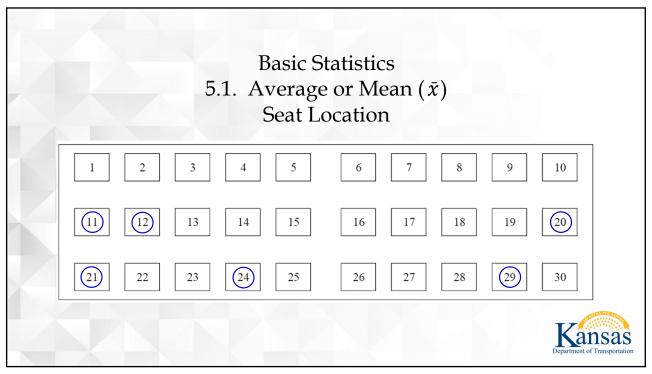
Kansas

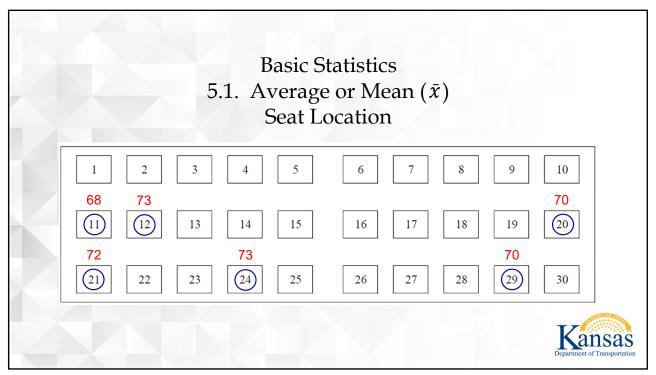






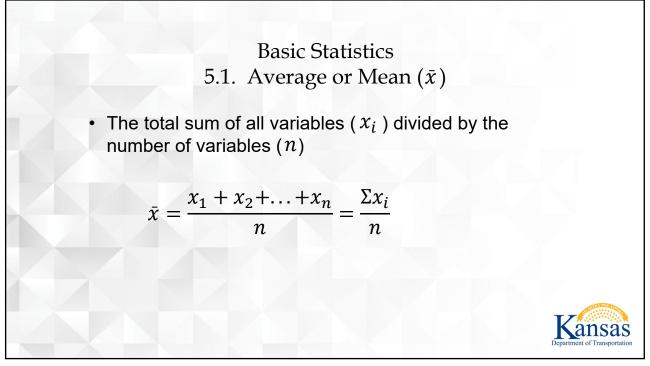
| | Basic Statistics | | |
|----------------|-----------------------------|--------|------------------------------|
| 5.1. | Average or Mean (\bar{x} |) | |
| Data Point | Random Location | Height | |
| Data Point | Seat Location (1-30) | (in) | |
| X_1 | 29 | | |
| X ₂ | 24 | | |
| X ₃ | 20 | | |
| X_4 | 11 | | |
| X_5 | 21 | | |
| X_6 | 12 | | V |
| | | | Department of Transportation |



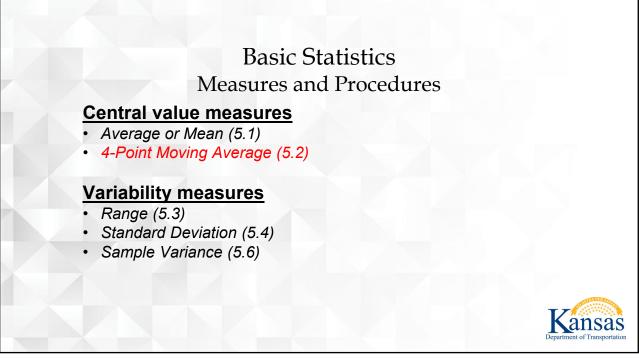


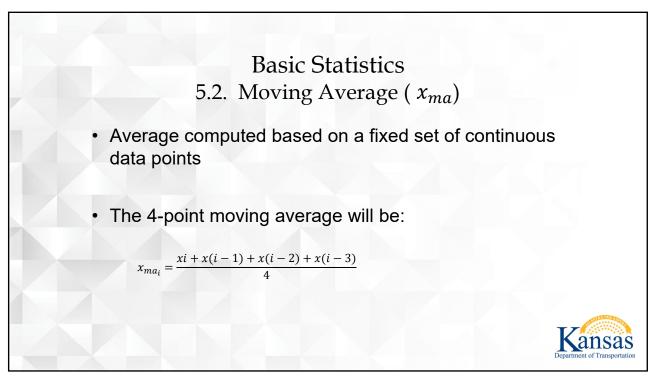
| | Basic Statistics | | |
|----------------|-----------------------------|--------|------------------------------|
| 5.1. | Average or Mean (\bar{x} |) | |
| Data Point | Random Location | Height | |
| Data Politi | Seat Location (1-30) | (in) | |
| X_1 | 29 | 70 | |
| X_2 | 24 | 73 | |
| X ₃ | 20 | 70 | |
| X_4 | 11 | 68 | |
| X_5 | 21 | 72 | |
| X_6 | 12 | 73 | Vanaaa |
| | | | Department of Transportation |

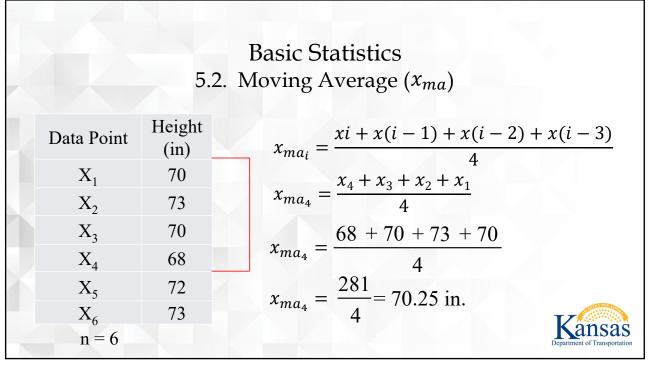
| 5.1. | Basic Stat Average o | | (\bar{x}) | |
|------|-------------------------|----------------|-------------|---|
| | Data Point | Height (in) | n = 6 | |
| | X_1 | 70 | | |
| | X_2 | 73 | | |
| | X ₃ | 70 | | |
| | X_4 | 68 | | |
| | X_5 | 72 | | |
| | X ₆ | 73 | | Kansas Department of Transportation |

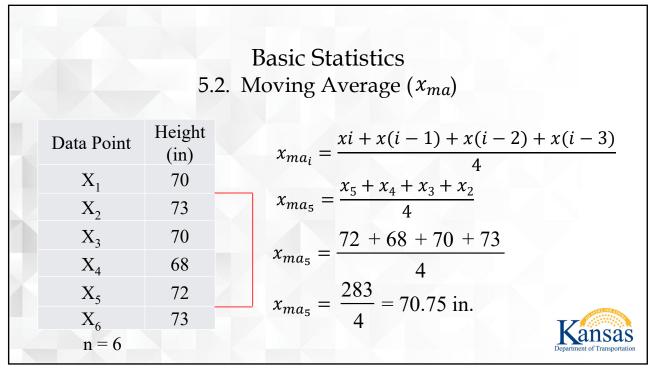


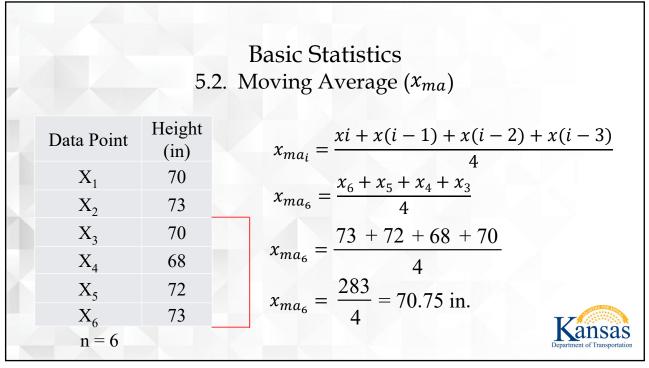
| | | Basic Statistics | |
|------------------|----------------|---|------------------------------|
| | 5. | 1. Average or Mean (\bar{x}) | |
| Data Point | Height (in) | $\bar{x} = \frac{x_1 + x_2 + x_3 + x_4 + x_5 + x_6}{x_1 + x_2 + x_3 + x_4 + x_5 + x_6}$ | |
| \mathbf{X}_{1} | 70 | n | |
| X ₂ | 73 | $\overline{70}$ 70 + 73 + 70 + 68 + 72 + 73 | |
| X ₃ | 70 | $x \equiv \frac{6}{6}$ | |
| X_4 | 68 | 126 | |
| X_5 | 72 | $\bar{x} = \frac{426}{6} = 71$ in. | |
| X_6 | 73 | 0 | TZ |
| n = 6 | 426 | | Department of Transportation |

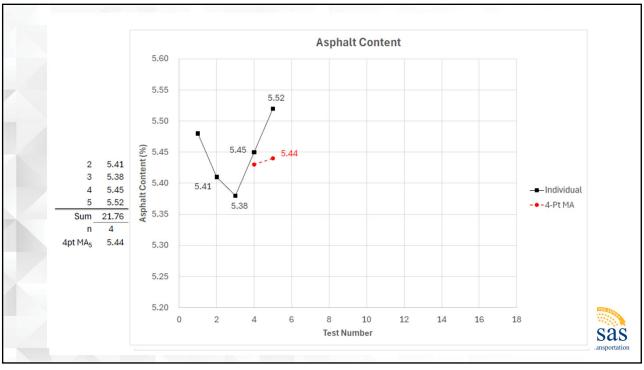


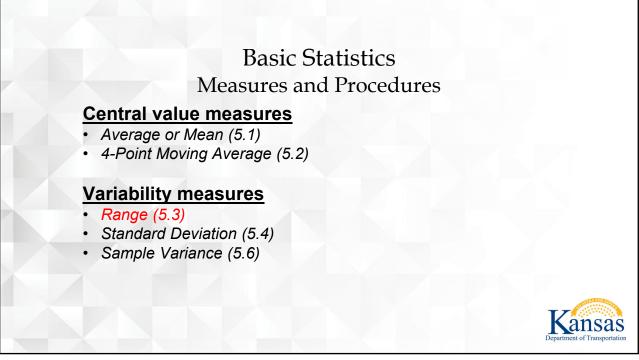


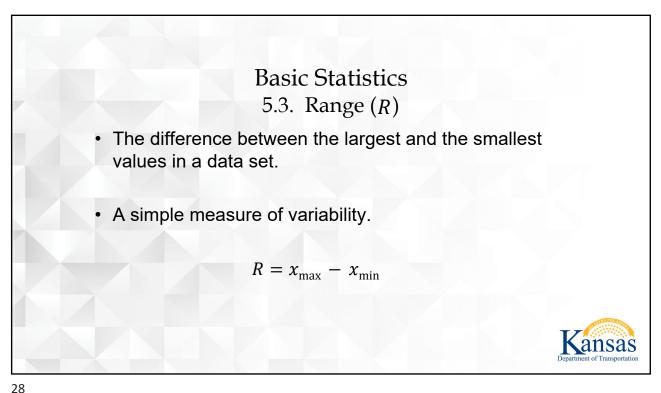


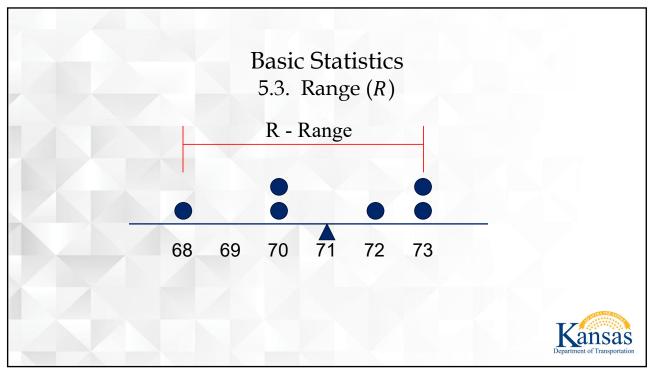




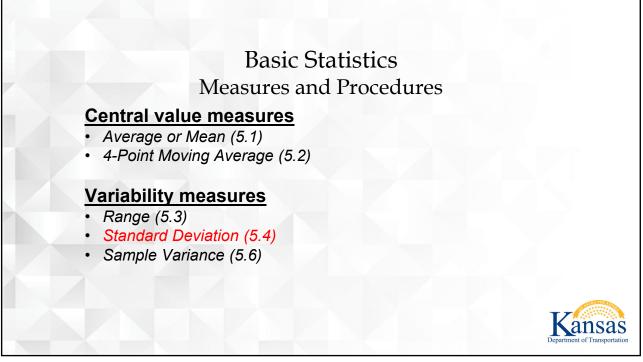


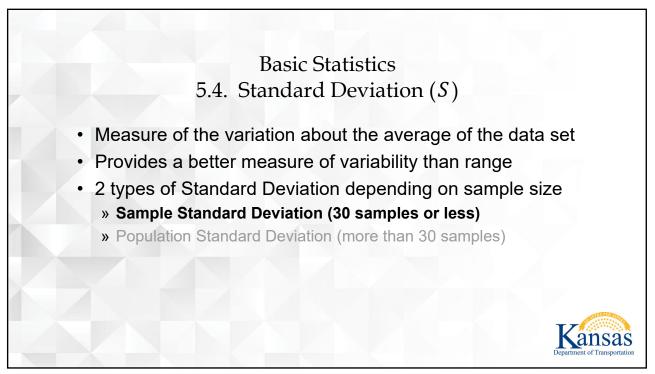


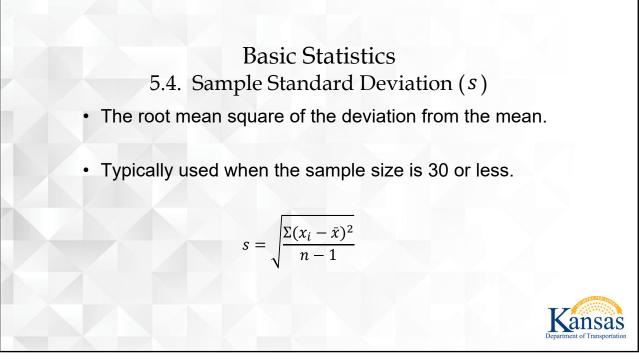


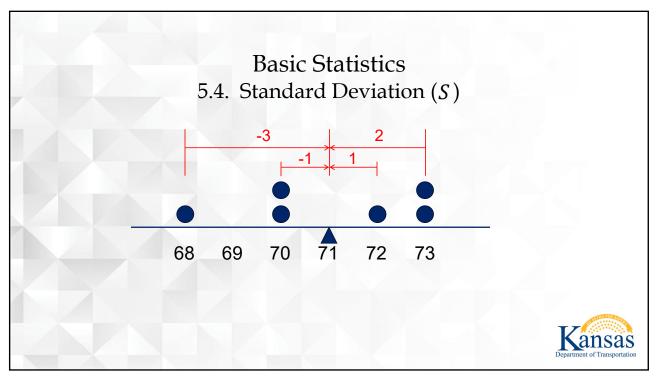


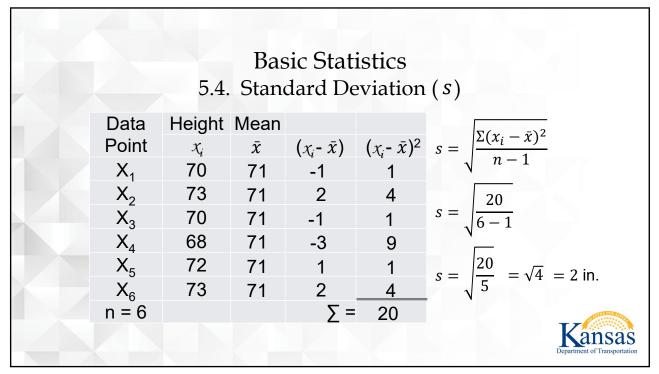
| Basic Statistics 5.3. Range (<i>R</i>) | | | | | |
|---|----------------|----------------|---------|---------------------------|------------------------------|
| | Data Point | Height (in) | Max/Min | $R = x_{\max} - x_{\min}$ | |
| | X_1 | 70 | | R = 73 - 68 | |
| | X_2 | 73 | Max | n = 75 - 00 | |
| | X_3 | 70 | | R = 5 in. | |
| | X_4 | 68 | Min | | |
| | X_5 | 72 | | | |
| | X ₆ | 73 | Max | | Kansas |
| | n = 6 | | | | Department of Transportation |

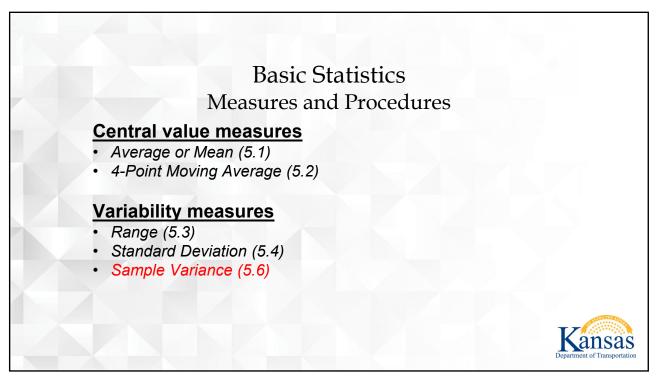


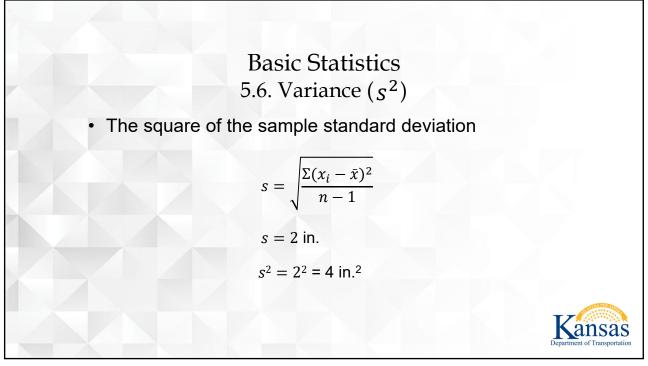


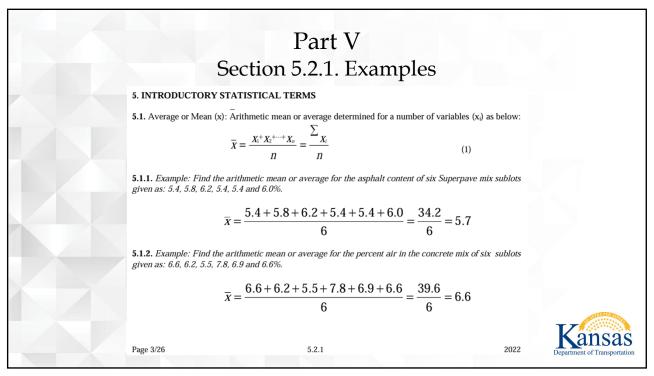


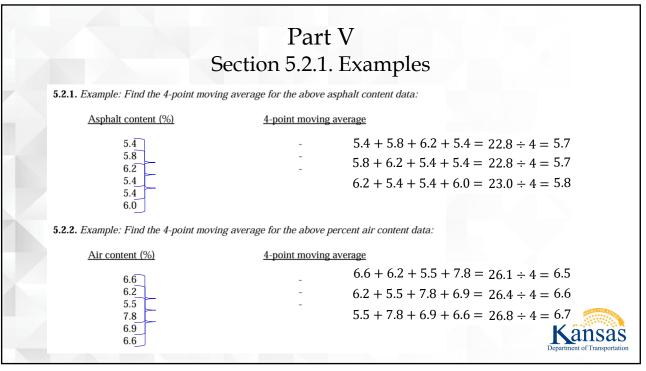


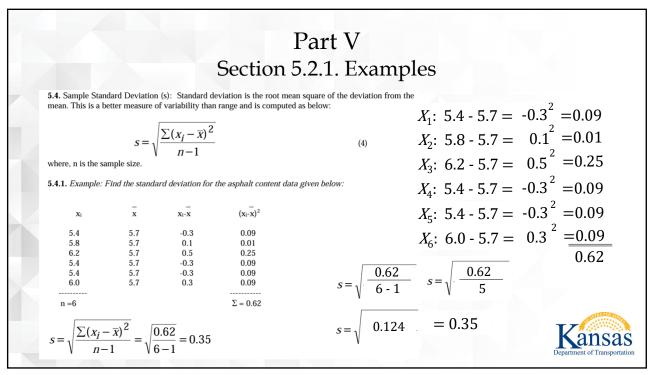


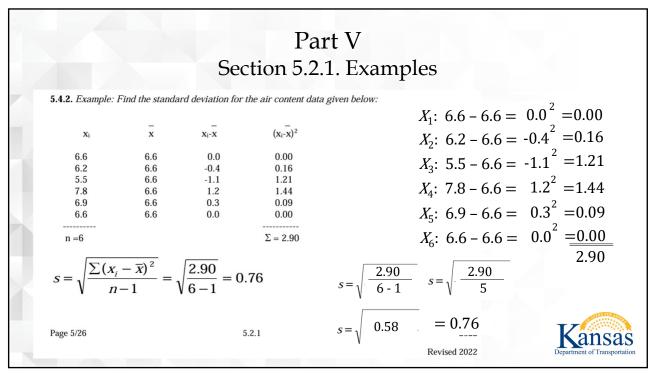


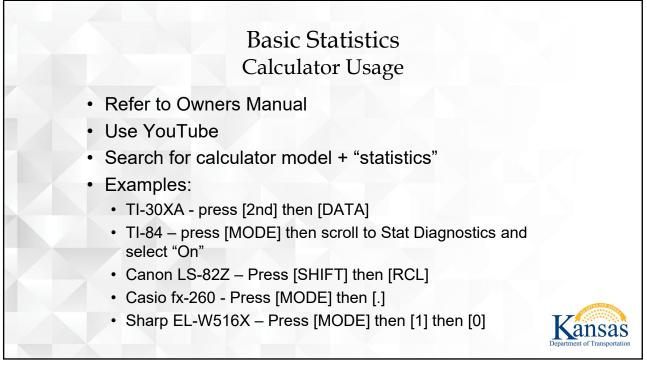


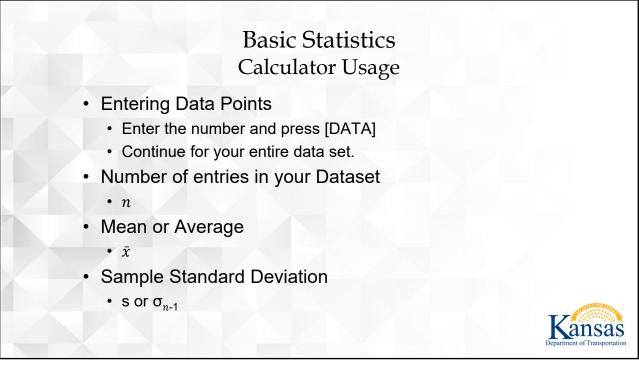


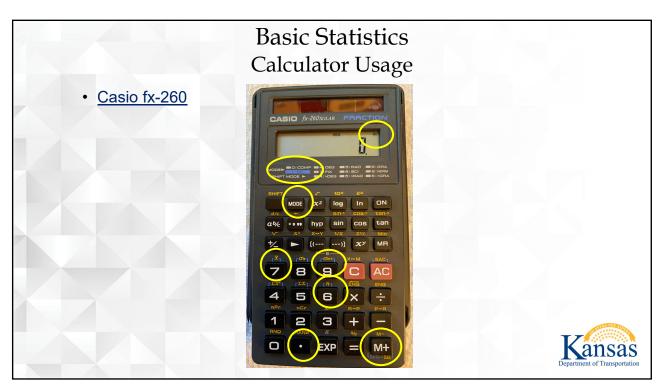


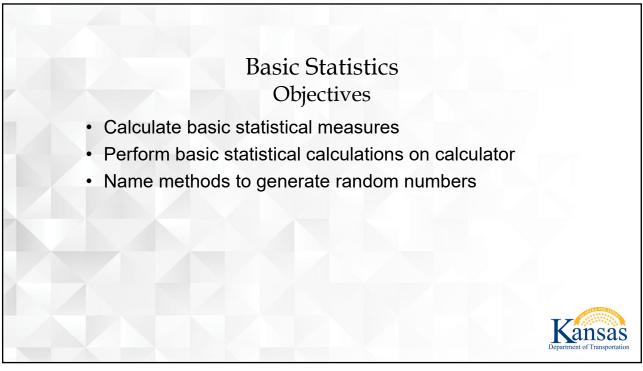


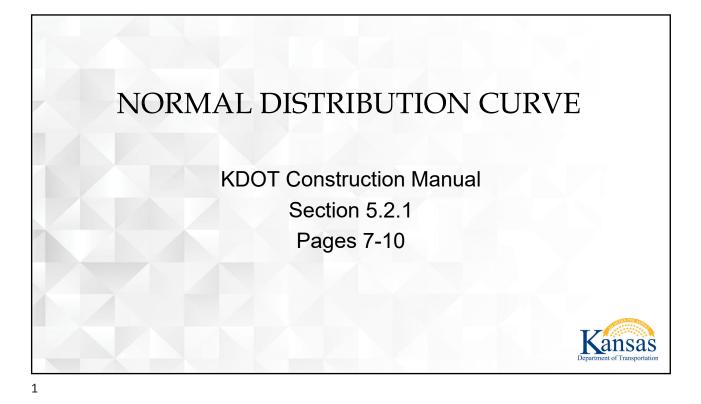


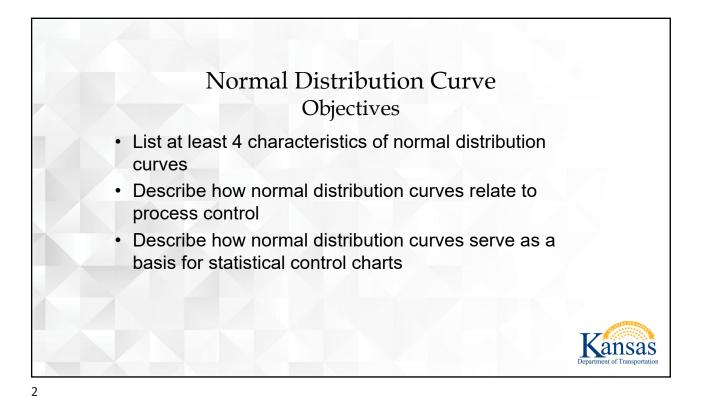


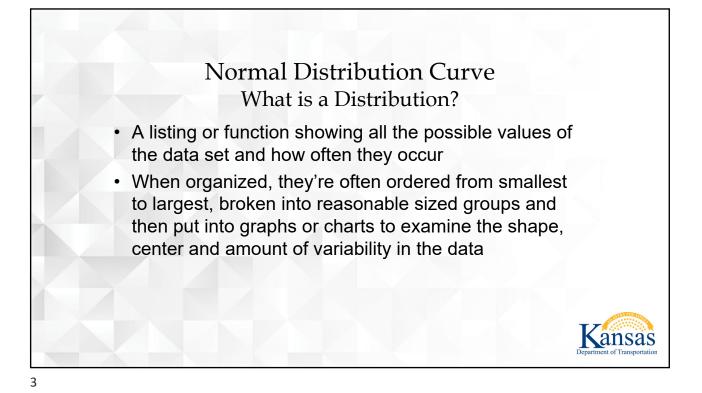


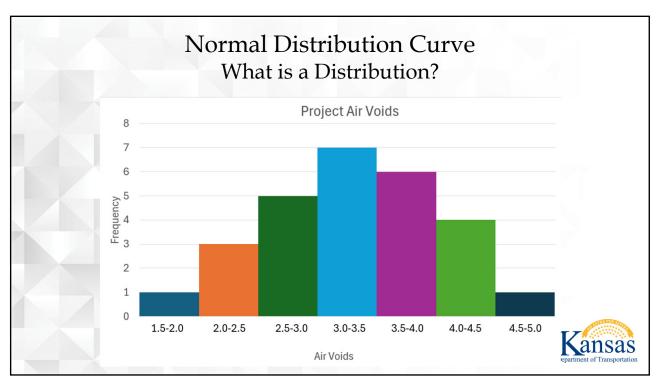


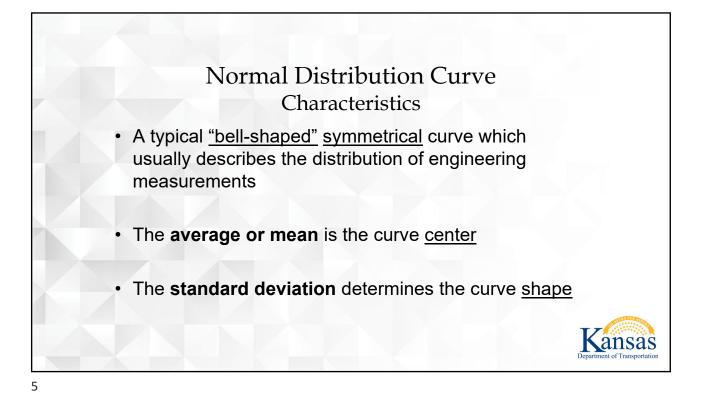


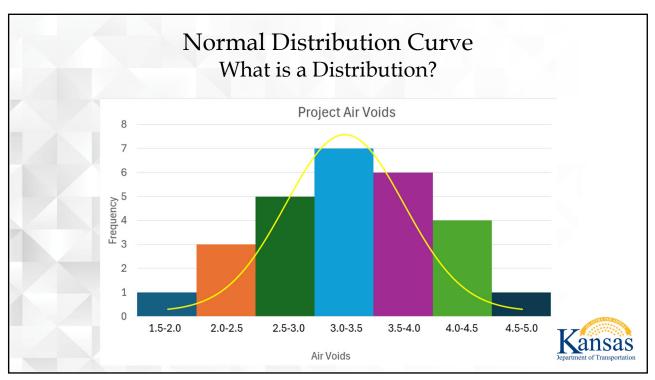


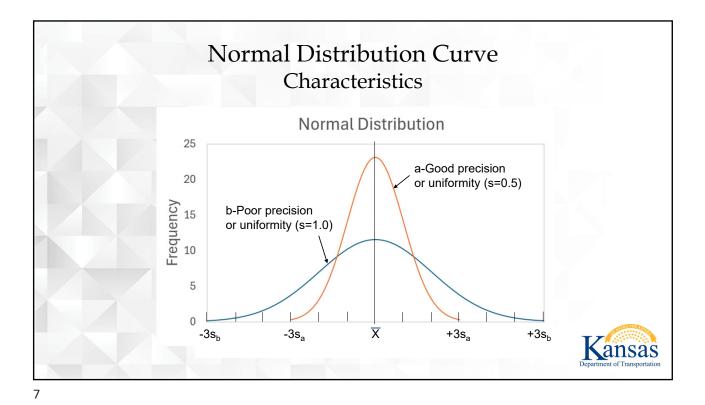


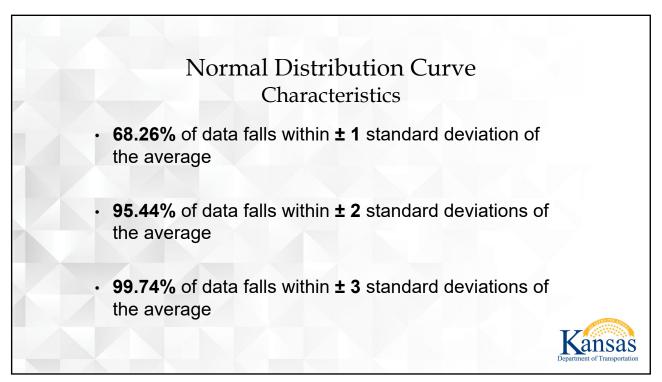


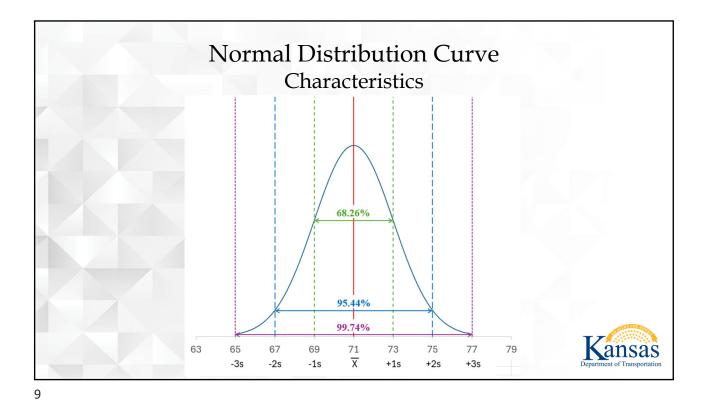


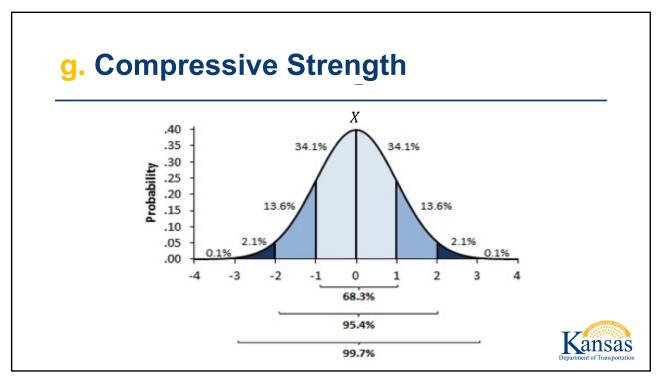


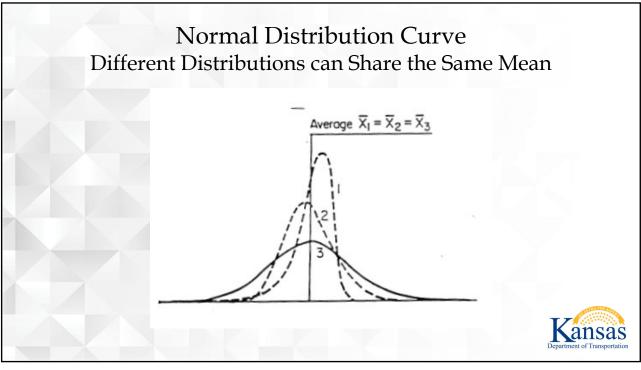


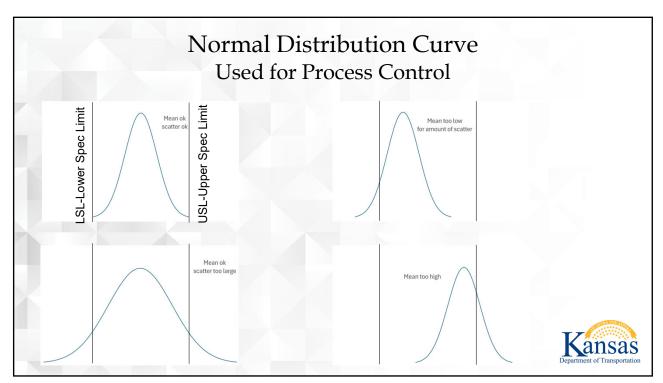


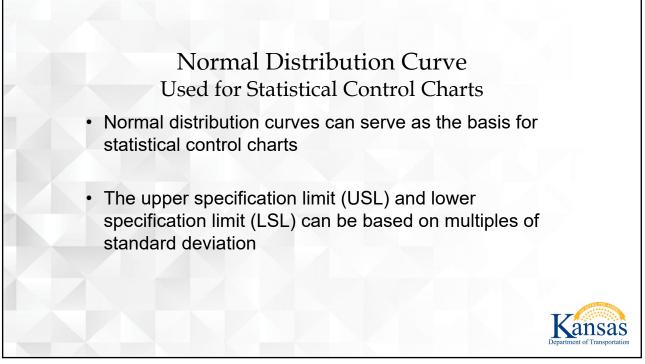


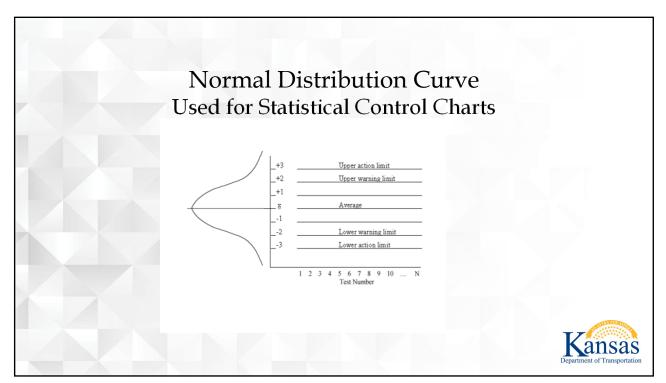


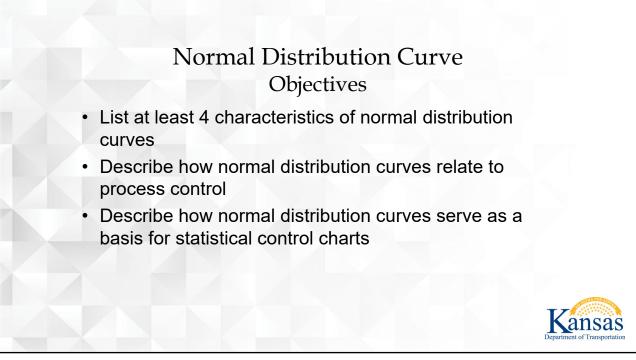


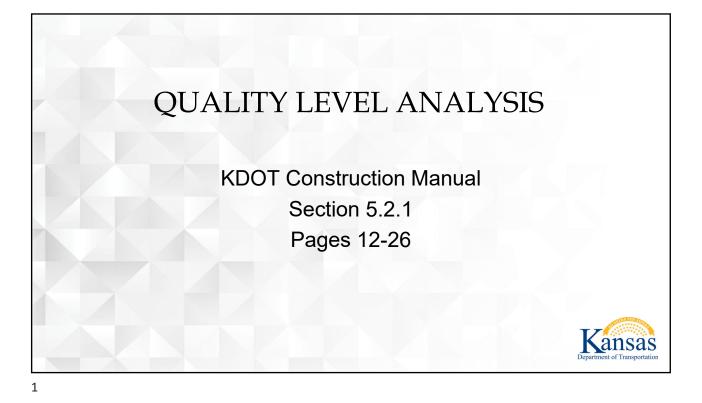


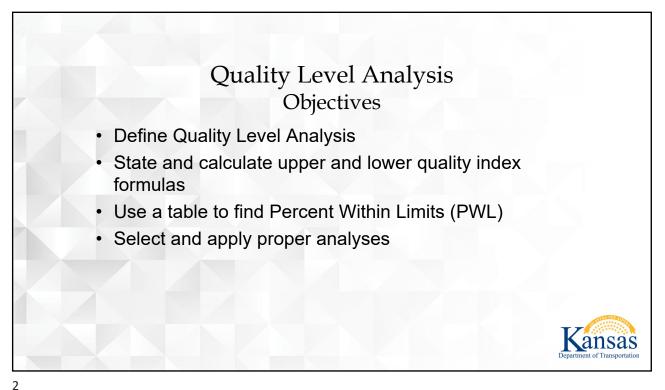


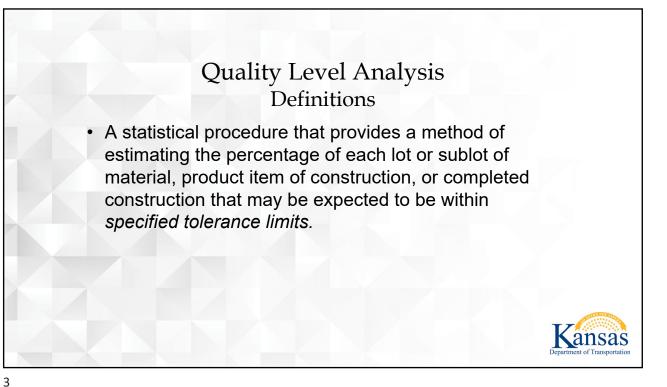


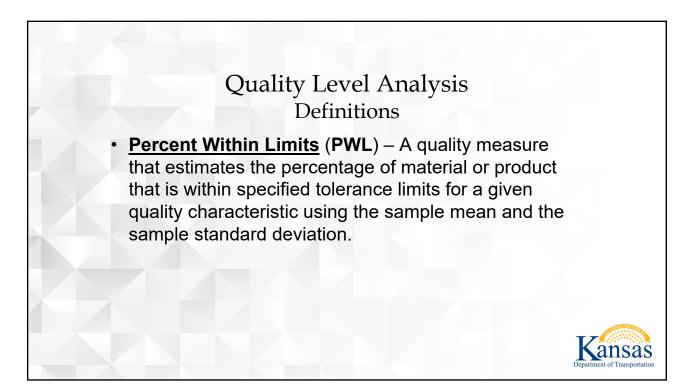


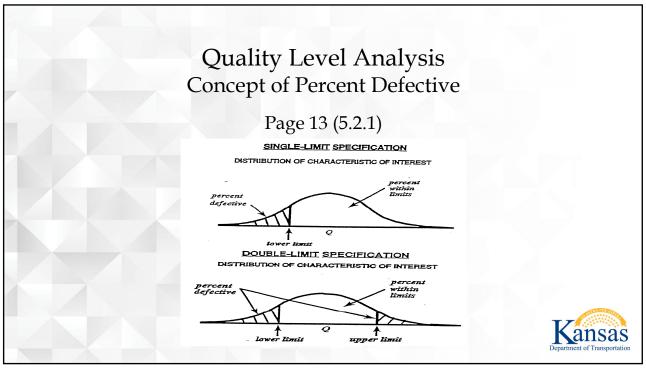


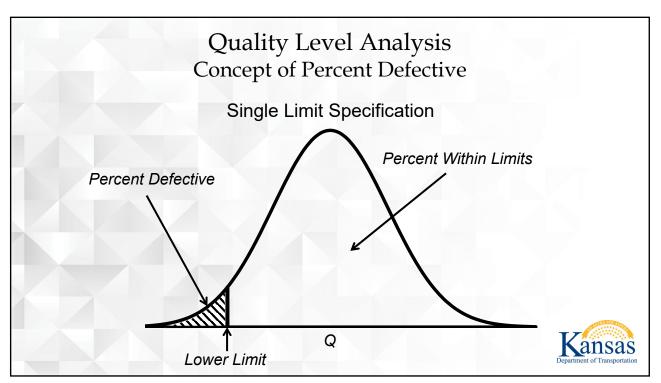


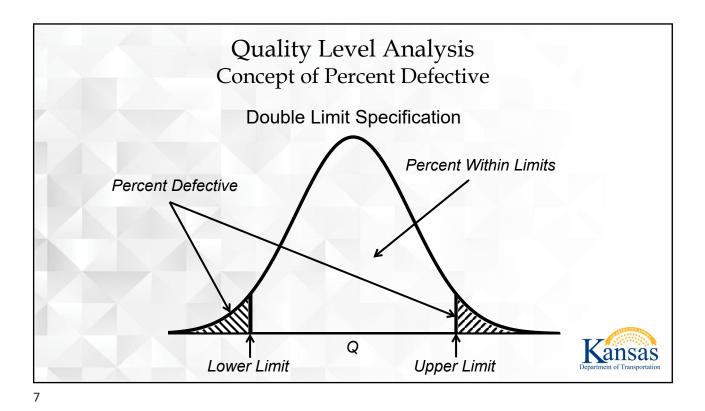


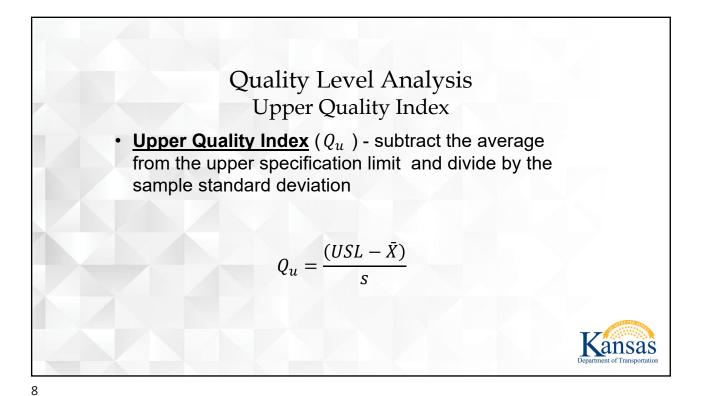


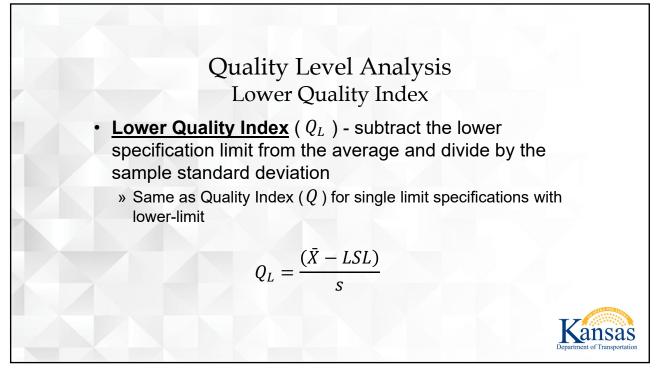


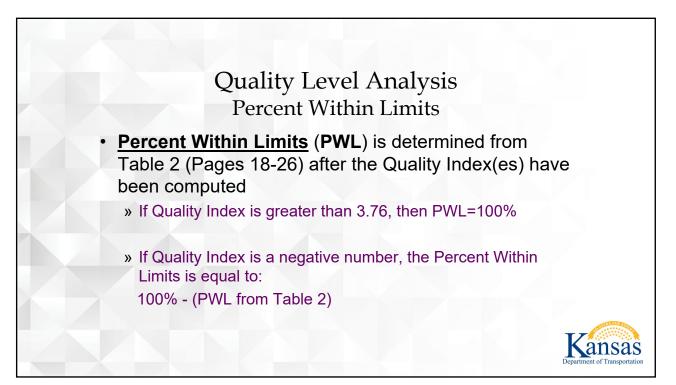


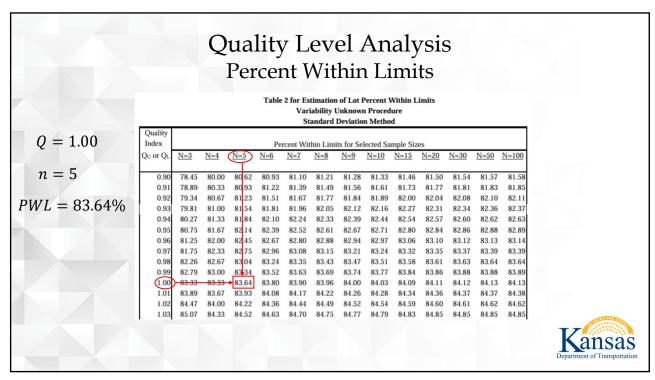










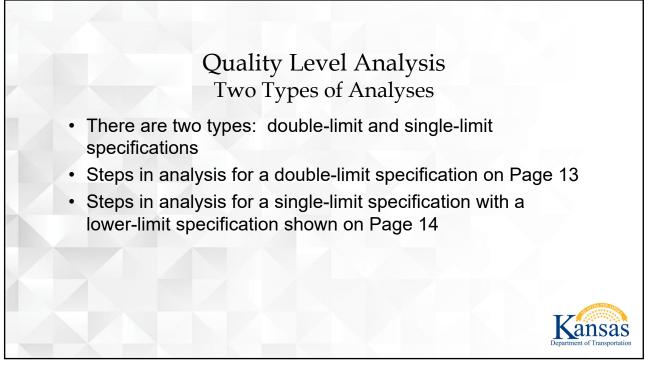


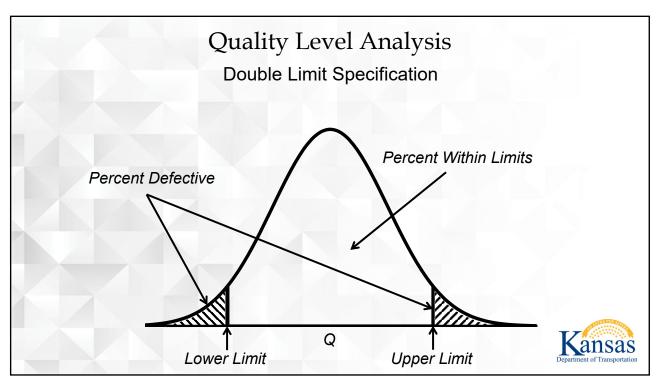
| | | | | Table | Vari | timation ability U | Jnknown | Proced | ure | imits | | | | | | |
|----------------------------------|------------|------------|------------|------------|-------|-----------------------|------------|-------------|-------------|-------------|-------------|-------------|--------------|---------|---------------|----|
| 0.1 | | | | | St | andard | Deviatio | n Metho | d | | | | | | | |
| Quality | | | | | | | | | | | | | | | | |
| Index | | | | | | hin Limi | | | 1 | | | | | | | |
| Q _U or Q _L | <u>N=3</u> | <u>N=4</u> | <u>N=5</u> | <u>N=6</u> | N=7 | <u>N=8</u> | <u>N=9</u> | <u>N=10</u> | <u>N=15</u> | <u>N=20</u> | <u>N=30</u> | <u>N=50</u> | <u>N=100</u> | | | |
| | | | | | | | | | | | | | | | | |
| 1.35 | 100.00 | 95.00 | 92.98 | 92.37 | 92.08 | 91.90 | 91.78 | 91.70 | 91.48 | 91.39 | 91.31 | 91.24 | 91.19 | | | |
| 1.36 | 100.00 | 95.33 | 93.21 | 92.58 | 92.27 | 92.09 | 91.96 | 91.88 | 91.65 | 91.56 | 91.47 | 91.40 | 91.35 | | | |
| 1.37 | 100.00 | 95.67 | 93.44 | 92.78 | 92.46 | 92.27 | 92.14 | 92.05 | 91.82 | 91.72 | 91.63 | 91.56 | 91.51 | | | |
| 1.38 | 100.00 | 96.00 | 93.67 | 92.98 | 92.65 | 92.45 | 92.32 | 92.23 | 91.99 | 91.88 | 91.79 | 91.72 | 91.67 | | | |
| 1.39 | 100.00 | 96.33 | 93.90 | 93.18 | 92.83 | 92.63 | 92.49 | 92.40 | 92.15 | 92.04 | 91.95 | 91.88 | 91.82 | | | |
| 1.40 | 100.00 | 96.67 | 94.12 | 93.37 | 93.02 | 92.81 | 92.67 | 92.56 | 92.31 | 92.20 | 92.10 | 92.03 | 91.98 | | | |
| 1.41 | 100.00 | 97.00 | 94.34 | 93.57 | 93.20 | 92.98 | 92.83 | 92.73 | 92.47 | 92.36 | 92.26 | 92.18 | 92.13 | | | |
| 1.42 | 100.00 | 97.33 | 94.56 | 93.76 | 93.38 | 93.15 | 93.00 | 92.90 | 92.63 | 92.51 | 92.41 | 92.33 | 92.27 | | | |
| 1.43 | 100.00 | 97.67 | 94.77 | 93.95 | 93.55 | 93.32 | 93.17 | 93.06 | 92.78 | 92.66 | 92.56 | 92.48 | 92.42 | | | |
| 1.44 | 100.00 | 98.00 | 94.98 | 94.13 | 93.73 | 93.49 | 93.33 | 93.22 | 92.93 | 92.81 | 92.70 | 92.62 | 92.56 | | | |
| 1.45 | 100.00 | 98.33 | 95.19 | 94.32 | 93.90 | 93.65 | 93.49 | 93.37 | 93.08 | 92.96 | 92.85 | 92.76 | 92.70 | | | |
| 1.46 | 100.00 | 98.67 | 95.40 | 94.50 | 94.07 | 93.81 | 93.65 | 93.53 | 93.23 | 93.10 | 92.99 | 92.90 | 92.84 | | | |
| 1.47 | 100.00 | 99.00 | 95.61 | 94.67 | 94.23 | 93.97 | 93.80 | 93.68 | 93.37 | 93.25 | 93.13 | 93.04 | 92.98 | | | |
| 1.48 | 100.00 | 99.33 | 95.81 | 94.85 | 94.40 | 94.13 | 93.96 | 93.83 | 93.52 | 93.39 | 93.27 | 93.18 | 93.12 | | | |
| 1.49 | 100.00 | 99.67 | 96.01 | 95.02 | 94.56 | 94.29 | 94.11 | 93.98 | 93.66 | 93.52 | 93.40 | 93.31 | 93.25 | | | |
| 1.50 | 100.00 | 100.00 | 96.20 | 95.19 | 94.72 | 94.44 | 94.26 | 94.13 | 93.80 | 93.66 | 93.54 | 93.45 | 93.38 | | | |
| 1.51 | 100.00 | 100.00 | 96.39 | 95.36 | 94.87 | 94.59 | 94.40 | 94.27 | 93.94 | 93.80 | 93.67 | 93.58 | 93.51 | | | |
| 1.52 | 100.00 | 100.00 | 96.58 | 95.53 | 95.03 | 94.74 | 94.55 | 94.41 | 94.07 | 93.93 | 93.80 | 93.71 | 93.64 | | | |
| 1.53 | 100.00 | 100.00 | 96.77 | 95.69 | 95.18 | 94.88 | 94.69 | 94.55 | 94.20 | 94.06 | 93.93 | 93.83 | 93.76 | | | |
| 1.54 | 100.00 | 100.00 | 96.95 | 95.85 | 95.33 | 95.03 | 94.83 | 94.69 | 94.33 | 94.19 | 94.05 | 93.96 | 93.89 | | | |
| 1.55 | 100.00 | 100.00 | 97.13 | 96.00 | 95.48 | 95.17 | 94.97 | 94.82 | 94.46 | 94.31 | 94.18 | 94.08 | 94.01 | | TRA PER | |
| 1.56 | 100.00 | 100.00 | 97.31 | 96.16 | 95.62 | 95.31 | 95.10 | 94.95 | 94.59 | 94.44 | 94.30 | 94.20 | 94.13 | | Sugar States | |
| 1.57 | 100.00 | 100.00 | 97.48 | 96.31 | 95.76 | 95.44 | 95.23 | 95.08 | 94.71 | 94.56 | 94.42 | 94.32 | 94.25 | | and | 00 |
| Page 21/ | 26 | | | | | 5.2.1 | | | | | | | 2022 | Departm | ans of Transp | as |
| | | | | | | | | | | | | Revis | ed 2022 | | | |

| | | | | | Var | iability I | Unknown | Percent V n Proced | | | | | | |
|------------------|-------------------|---------------------|----------------------|--------------------|------------|-------------------|---------------------|-----------------------|-------------|---------------|-------------|-------------|---------------------------------|---------------|
| Quality | | | | | S | andard | Deviatio | n Metho | a | | | | _ | |
| Quality Index | | | | P | | | | | 1.0 | | | | | Dage 26 of 20 |
| | | | | | | | | lected Sa | | | | 11 50 | | Page 26 of 26 |
| QU or QL | <u>N=3</u> | <u>N=4</u> | <u>N=5</u> | <u>N=6</u> | <u>N=7</u> | <u>N=8</u> | <u>N=9</u> | <u>N=10</u> | <u>N=15</u> | <u>N=20</u> | <u>N=30</u> | <u>N=50</u> | <u>N=100</u> | 5.2.1 |
| 3.60 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 99.99 | 99.99 | |
| 3.61 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 99.99 | 99.99 | |
| 3.62 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 99.99 | |
| 3.63 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 99.99 | |
| 3.64 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 99.99 | |
| 3.65 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 99.99 | |
| 3.66 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 99.99 | |
| 3.67 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 99.99 | |
| 3.68 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 99.99 | |
| 3.69 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 99.99 | |
| 3.70 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 99.99 | |
| 3.71 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 99.99 | |
| 3.72 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 99.99 | |
| 3.73 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 99.99 | |
| 3.74 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 99.99 | |
| 3.75 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 99.99 | |
| 3.76 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | |
| integratii | ng the b PWL f | eta dist rom the | ribution e tables | n functi , comp | on corr | espond from th | ing to Q ne samp | Quality | Index (| Q) and sample | Sample | Size (N | umerically v). ation with | Kansa |



| | | | | | | | Ar n L | | ysi its | s | | | | | |
|-----------------------|----------------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|----------------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|------------|
| $Q_L = -0.55$ | | | | | Table | Var | iability U | Inknown | Percent V n Proced n Metho | ure | imits | | | | |
| n = 4 | Quality Index | | | | Po | rcont Wit | hin Limi | ts for Sel | lected Sa | mple Siz | 95 | | | | |
| Enter Table 2 with: | Q _U or Q _L | | <u>N=4</u> | <u>N=5</u> | <u>N=6</u> | <u>N=7</u> | <u>N=8</u> | <u>N=9</u> | <u>N=10</u> | <u>N=15</u> | <u>N=20</u> | <u>N=30</u> | <u>N=50</u> | <u>N=100</u> | |
| $Q_L = 0.55$ | 0.45 0.46 0.47 | 62.74 63.04 63.34 | 65.00 65.33 65.67 | 65.84 66.19 66.53 | 66.27 66.62 66.96 | 66.51 66.87 67.22 | 66.67 67.03 67.38 | 66.79 67.14 67.49 | 66.87 67.22 67.58 | 67.08 67.43 67.79 | 67.16 67.52 67.88 | 67.24 67.60 67.96 | 67.29 67.65 68.01 | | |
| | 0.48 0.49 | 63.65 63.95 | 66.00 66.33 | 66.88 67.22 | 67.31 67.66 | 67.57 67.92 | 67.73 68.08 | 67.85 68.20 | 67.93 68.28 | 68.15 68.50 | 68.23 68.59 | 68.31 68.67 | 68.37 68.72 | 68.40 68.76 | |
| $PWL_{L} = 68.33$ | 0.50 0.51 0.52 | 64.25 64.56 64.87 | 66.67 67.00 67.33 | 67.56 67.90 68.24 | 68.00 68.35 68.69 | 68.26 68.61 68.96 | 68.43 68.78 69.13 | 68.55 68.90 69.24 | 68.63 68.98 69.33 | 68.85 69.20 69.55 | 68.94 69.29 69.64 | 69.02 69.37 69.72 | 69.07 69.43 69.77 | 69.11 69.46 69.81 | |
| | 0.53 0.54 | 65.18 65.49 | 67.67 68,00 | 68.58 68.92 | 69.04 69.38 | 69.30 69.64 | 69.47 69.82 | 69.59 69.93 | 69.68 70.02 | 69.90 70.24 | 69.99 70.33 | 70.07 70.41 | 70.12 70.47 | 70.51 | |
| $PWL_L = 100 - 68.33$ | 0.55 0.56 0.57 | 65.80 66.12 66.43 | 68.33 68.67 69.00 | 69.26 69.60 69.94 | 69.72 70.06 70.40 | 69.99 70.33 70.67 | 70.16 70.50 70.84 | 70.28 70.62 70.96 | 70.36 70.71 71.05 | 70.59 70.93 71.27 | 70.68 71.02 71.36 | 70.76 71.10 71.44 | 70.81 71.15 71.49 | 70.85 71.19 71.53 | |
| $PWL_L = 31.67$ | 0.58 | 66.75 67.07 | 69.33 69.67 | 70.27 70.61 | 70.74 71.07 | 71.01 71.34 | 71.18 71.52 | 71.30 71.64 | 71.39 71.72 | 71.61 71.95 | 71.70 72.04 | 71.78 72.11 | 71.43 71.83 72.17 | 71.87 72.21 | ST.STRA |
| | | | | | | | | | | | | | | Ka | n of Tr |





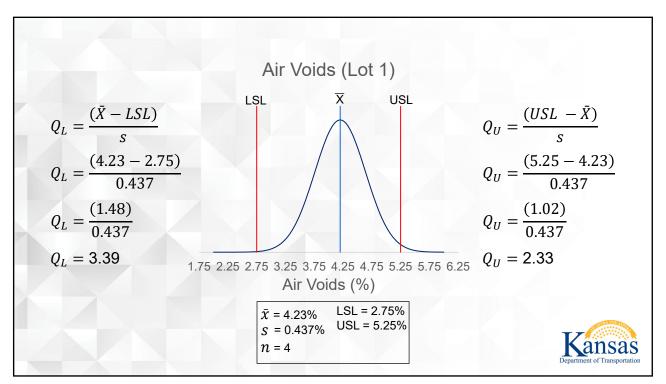
Quality Level Analysis Double Limit Specification

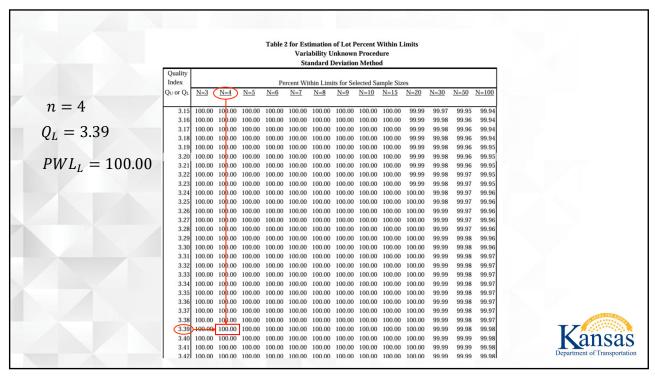
6.5.

A contractor has run air voids tests on five lots of SM-19B. The specification limits for air voids are 4 ± 1.25 %. This sets the lower specification limit (LSL) at 2.75 % (4 - 1.25 %) air voids and the upper specification limit (USL) at 5.25 % (4 + 1.25 %) air voids. Conduct a Quality Level Analysis and compute the percent within limits.

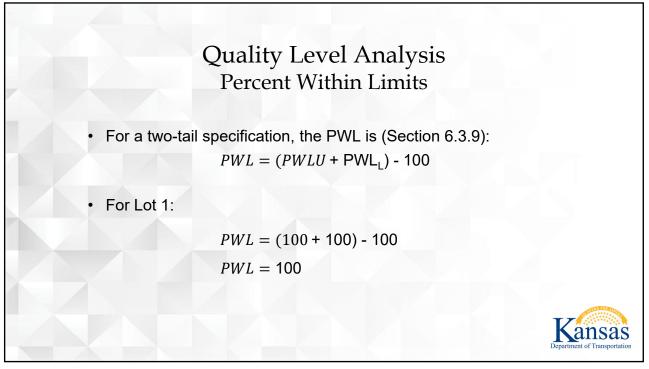
| Lot 1 | Sublot 1A 1B 1C 1D | Percent Air Voids 4.30 3.77 4.05 4.80 | $\bar{x} = 4.23\%$ s = 0.437% n = 4 | LSL = 2.75% USL = 5.25% | |
|----------|--------------------------------|---|---|----------------------------|--|
| 2 | 2A 2B 2C | 4.90 5.07 3.82 | | | A CONTRACTOR OF CONTRACTOR |
| | 20 2D | 3.53 | | | Kansa Department of Transpor |

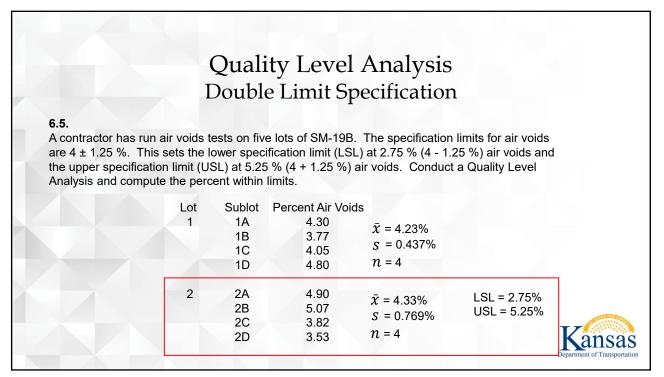
17

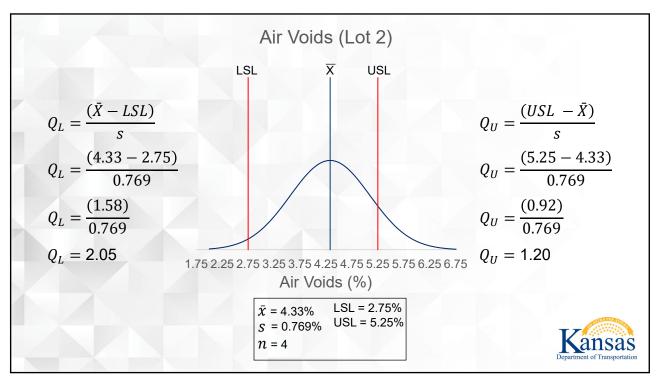


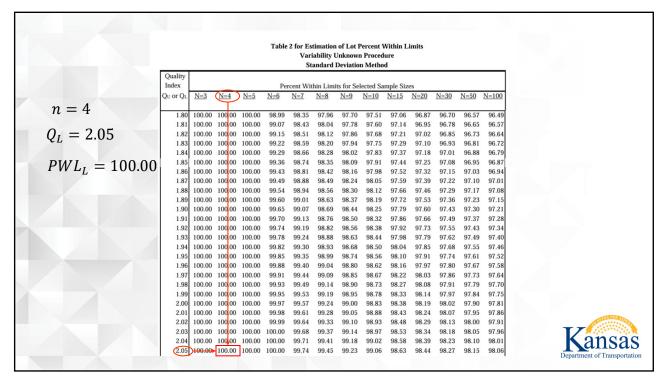


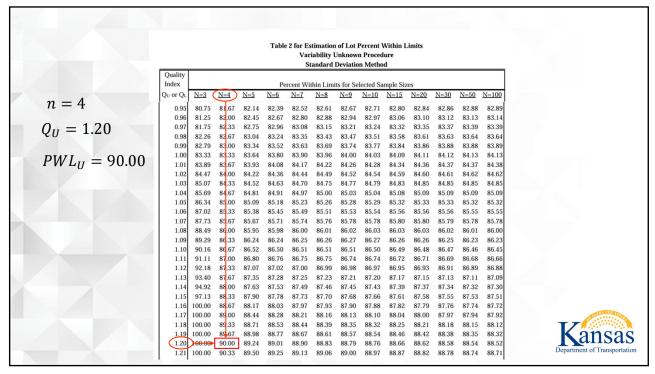
| | | | | | | | | 57 | | | | | | 6 | |
|------------------|------------------------------|------------------|----------------------------|----------------------------|----------------------------|----------------------------|------------------------------------|--------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|------------------------------|
| | | | | | Table | Var | timation iability U andard I | Inknown | Proced | ure | imits | | | | |
| n = 4 | Quality Index QU or QL | <u>N=3</u> | <u>N=4</u> | <u>N=5</u> | Per <u>N=6</u> | rcent Wit | hin Limi <u>N=8</u> | ts for Sel <u>N=9</u> | ected Sa <u>N=10</u> | mple Siz <u>N=15</u> | es <u>N=20</u> | <u>N=30</u> | <u>N=50</u> | <u>N=100</u> | |
| $Q_U = 2.33$ | 2.25 2.26 | | | 100.00 100.00 | 100.00 100.00 | 100.00 100.00 | 99.91 99.92 | 99.79 99.80 | 99.68 99.70 | 99.34 99.37 | 99.18 99.21 | 99.04 99.07 | 98.93 98.96 | 98.85 98.88 | |
| $PWL_U = 100.00$ | 2.27 2.28 2.29 | 100.00 | 100.00 | 100.00 100.00 100.00 | 100.00 100.00 100.00 | 100.00 100.00 100.00 | 99.93 99.94 99.95 | 99.82 99.83 99.85 | 99.71 99.73 99.75 | 99.39 99.42 99.44 | 99.24 99.26 99.29 | 99.10 99.12 99.15 | 98.99 99.02 99.05 | 98.91 98.94 98.97 | |
| | 2.30 2.31 2.32 | 100.00 | 100.00 100.00 100.00 | 100.00 100.00 | 100.00 100.00 100.00 | 100.00 100.00 100.00 | 99.96 99.96 99.97 | 99.86 99.87 99.89 | 99.77 99.78 99.80 | 99.46 99.48 99.51 | 99.32 99.34 99.36 | 99.18 99.20 99.23 | 99.07 99.10 99.13 | 99.00 99.03 99.05 | |
| | 2.33 2.34 2.35 | 100.00 | 100.00 | | 100.00 100.00 100.00 | 100.00 100.00 100.00 | 99.98 99.98 99.98 | 99.90 99.91 99.92 | 99.81 99.82 99.84 | 99.53 99.55 99.57 | 99.39 99.41 99.43 | 99.25 99.28 99.30 | 99.15 99.18 99.20 | 99.08 99.10 99.13 | |
| | 2.36 2.37 2.38 | 100.00 100.00 | 100.00 100.00 100.00 | 100.00 100.00 100.00 | 100.00 100.00 100.00 | 100.00 100.00 100.00 | 99.99 99.99 99.99 | 99.92 99.93 99.94 | 99.85 99.86 99.87 | 99.58 99.60 99.62 | 99.45 99.47 99.49 | 99.32 99.34 99.37 | 99.22 99.25 99.27 | 99.15 99.18 99.20 | |
| | 2.39 2.40 2.41 | 100.00 100.00 | 100.00 100.00 100.00 | 100.00 100.00 100.00 | 100.00 100.00 100.00 | 100.00 100.00 100.00 | 100.00 100.00 100.00 | 99.95 99.95 99.96 | 99.88 99.89 99.90 | 99.64 99.65 99.67 | 99.51 99.53 99.55 | 99.39 99.41 99.43 | 99.29 99.31 99.33 | 99.22 99.25 99.27 | |
| | 2.42 2.43 2.44 | 100.00 100.00 | 100.00 100.00 100.00 | 100.00 100.00 100.00 | 100.00 100.00 100.00 | 100.00 100.00 100.00 | 100.00 100.00 100.00 | 99.96 99.97 99.97 | 99.91 99.92 99.92 | 99.68 99.70 99.71 | 99.56 99.58 99.60 | 99.44 99.46 99.48 | 99.35 99.37 99.39 | 99.29 99.31 99.33 | V |
| | 2.45 | | | | 100.00 | 100.00 | 100.00 | 99.98 | 99.93 | 99.73 | 99.61 | 99.50 | 99.41 | 99.35 | Department of Transportation |

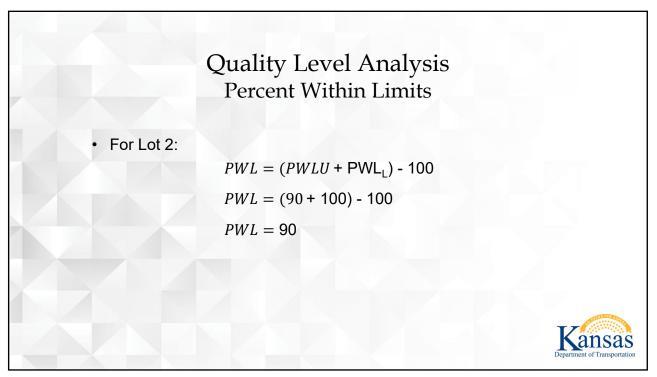


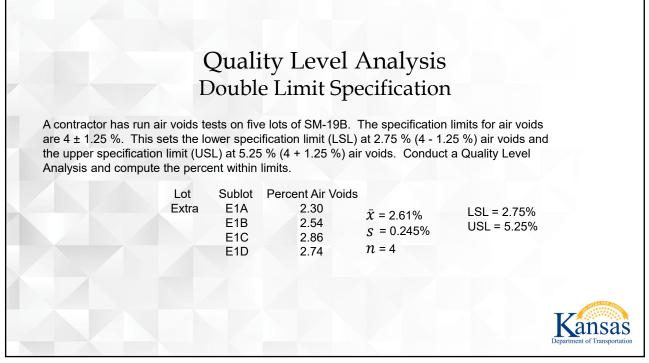


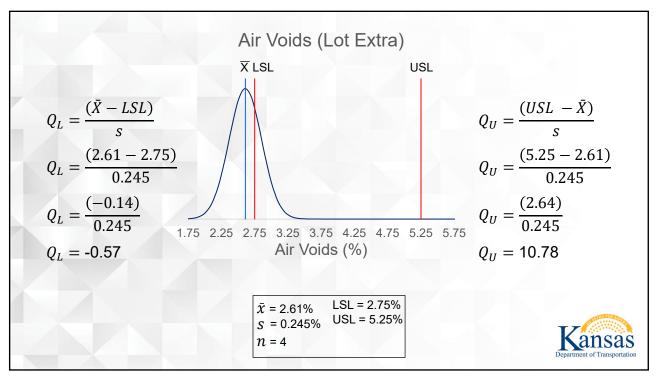




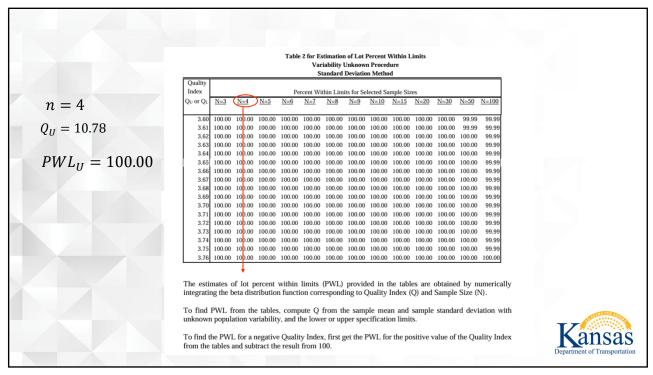


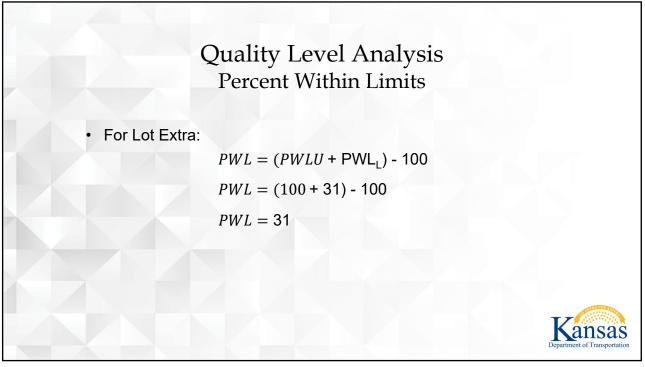


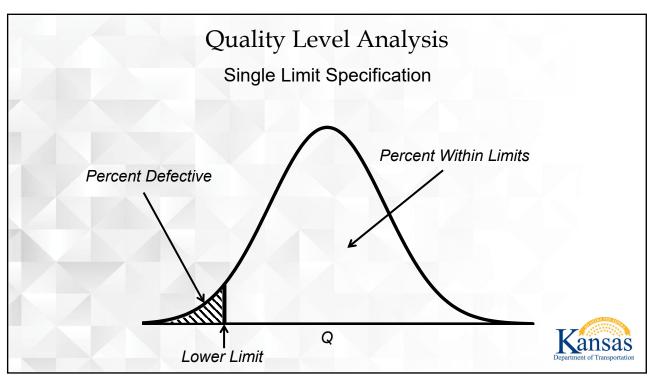




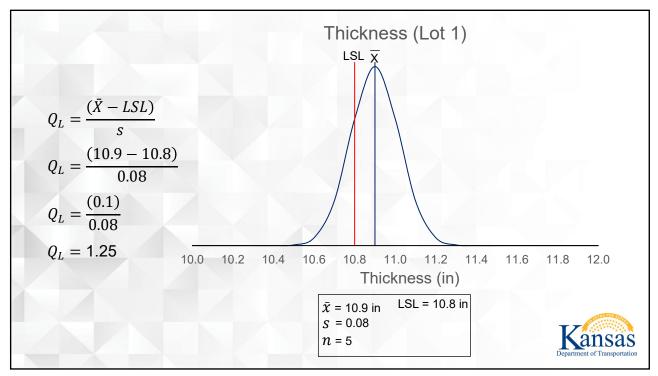
| n = 4 | | | | | Table | Vari | iability U | Jnknown | Percent V n Proced n Metho | ure | imits | | | |
|--------------------------|-------------------|----------------|----------------------|----------------|----------------|----------------|-----------------|-------------------|----------------------------------|------------------|----------------|----------------|----------------|----------------|
| | Quality | | | | 5 | | | | 10 | 1.0 | | | | |
| $Q_{L} = -0.57$ | Index Ou or OL | N=3 | N=4 | N=5 | Per N=6 | N=7 | hin Limi N=8 | ts for Sel N=9 | lected Sa N=10 | mple Siz N=15 | es N=20 | N=30 | N=50 | N=100 |
| | | | | | | | | | | | | | | |
| | 0.45 | 62.74 | 65,00 | 65.84 | 66.27 | 66.51 | 66.67 | 66.79 | 66.87 | 67.08 | 67.16 | 67.24 | 67.29 | 67.33 |
| Go into table with: | 0.46 | 63.04 63.34 | 65.33 65.67 | 66.19 66.53 | 66.62 66.96 | 66.87 67.22 | 67.03 67.38 | 67.14 67.49 | 67.22 67.58 | 67.43 67.79 | 67.52 67.88 | 67.60 67.96 | 67.65 68.01 | 67.69 68.05 |
| $Q_L = 0.57$ | 0.47 | 63.65 | 66,00 | 66.88 | 67.31 | 67.57 | 67.73 | 67.85 | 67.93 | 68.15 | 68.23 | 68.31 | 68.37 | 68.40 |
| $Q_L = 0.07$ | 0.49 | 63.95 | 66 <mark>.</mark> 33 | 67.22 | 67.66 | 67.92 | 68.08 | 68.20 | 68.28 | 68.50 | 68.59 | 68.67 | 68.72 | |
| $PWL_{L} = 69.00$ | 0.50 | 64.25 | 66 <mark>.</mark> 67 | 67.56 | 68.00 | 68.26 | 68.43 | 68.55 | 68.63 | 68.85 | 68.94 | 69.02 | 69.07 | 69.11 |
| $I V L_L = 09.00$ | 0.51 0.52 | 64.56 64.87 | 67.00 67.33 | 67.90 68.24 | 68.35 68.69 | 68.61 68.96 | 68.78 69.13 | 68.90 69.24 | 68.98 69.33 | 69.20 69.55 | 69.29 69.64 | 69.37 69.72 | 69.43 69.77 | 69.46 69.81 |
| for | 0.53 | 65.18 | 67.67 | 68.58 | 69.04 | 69.30 | 69.47 | 69.59 | 69.68 | 69.90 | 69.99 | 70.07 | 70.12 | 70.16 |
| | 0.54 | 65.49 | 68 <mark>.</mark> 00 | 68.92 | 69.38 | 69.64 | 69.82 | 69.93 | 70.02 | 70.24 | 70.33 | 70.41 | 70.47 | 70.51 |
| $Q_L = 0.57$ | 0.55 | 65.80 | 68.33 | 69.26 | 69.72 | 69.99 | 70.16 | 70.28 | 70.36 | 70.59 | 70.68 | 70.76 | 70.81 | 70.85 |
| | 0.56 | 66.12 | 68,67 69.00 | 69.60 69.94 | 70.06 70.40 | 70.33 70.67 | 70.50 70.84 | 70.62 70.96 | 70.71 71.05 | 70.93 71.27 | 71.02 71.36 | 71.10 71.44 | 71.15 71.49 | 71.19 71.53 |
| however, | 0.58 | 66.75 | 69.33 | 70.27 | 70.74 | 71.01 | 71.18 | 71.30 | 71.39 | 71.61 | 71.70 | 71.78 | 71.83 | |
| $Q_L = -0.57$ | 0.59 | 67.07 | 69.67 | 70.61 | 71.07 | 71.34 | 71.52 | 71.64 | 71.72 | 71.95 | 72.04 | 72.11 | 72.17 | 72.21 |
| $Q_L = 0.57$ | 0.60 | 67.39 | 70.00 70.33 | 70.95 71.28 | 71.41 71.75 | 71.68 72.02 | 71.85 72.19 | 71.97 72.31 | 72.06 72.40 | 72.28 72.61 | 72.37 72.70 | 72.45 72.78 | 72.50 72.84 | 72.54 72.87 |
| SO, | 0.61 | 67.72 68.04 | 70.33 | 71.28 | 72.08 | 72.02 | 72.19 | 72.31 | 72.40 | 72.95 | 73.04 | 73.11 | 72.84 | 73.20 |
| | 0.63 | 68.37 | 71.00 | 71.95 | 72.41 | 72.68 | 72.85 | 72.97 | 73.06 | 73.28 | 73.37 | 73.44 | 73.50 | 73.53 |
| $PWL_L = 100.00 - 69.00$ | 0.64 | 68.70 | 71.33 | 72.28 | 72.74 | 73.01 | 73.18 | 73.30 | 73.39 | 73.61 | 73.69 | 73.77 | 73.82 | 73.86 |
| 24.00 | 0.65 | 69.03 | 71.67 72.00 | 72.61 72.94 | 73.08 | 73.34 73.67 | 73.51 | 73.63 73.96 | 73.72 | 73.93 | 74.02 74.34 | 74.10 74.42 | 74.15 74.47 | 74.18 |
| $PWL_L = 31.00$ | 0.66 | 69.37 69.70 | 72.00 | 72.94 | 73.40 73.73 | 73.67 | 73.84 74.17 | 73.96 | 74.04 74.37 | 74.26 74.58 | 74.34 74.67 | 74.42 74.74 | 74.47 | 74.51 74.83 |
| | 0.68 | 70.04 | 72.67 | 73.60 | 74.06 | 74.32 | 74.49 | 74.61 | 74.69 | 74.90 | 74.99 | 75.06 | 75.11 | 75.14 |
| | 0.69 | 70.39 | 73.00 | 73.93 | 74.39 | 74.65 | 74.81 | 74.93 | 75.01 | 75.22 | 75.30 | 75.38 | 75.43 | 75.46 |



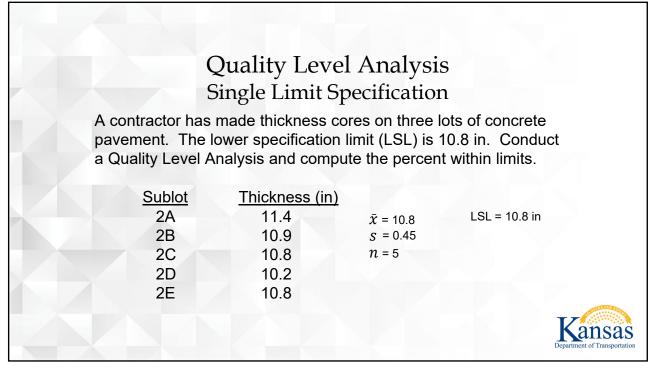


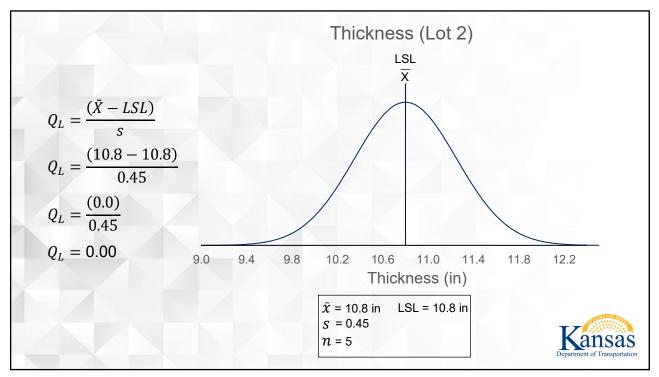


| | Quality Level | | | |
|--------------------------------------|--|-------------------------------------|------------------|---------------------------------|
| | Single Limit Sp | ecification | l | |
| pavement. The | is made thickness cor e lower specification li Analysis and comput | mit (LSL) is | 10.8 in. Conduct | |
| Sublot 1A 1B 1C 1D 1E | <u>Thickness (in)</u> 10.9 10.8 10.9 11.0 11.0 11.0 | $ \bar{x} = 10.9 s = 0.08 n = 5 $ | LSL = 10.8 in | |
| | | | K | ansas ment of Transportation |

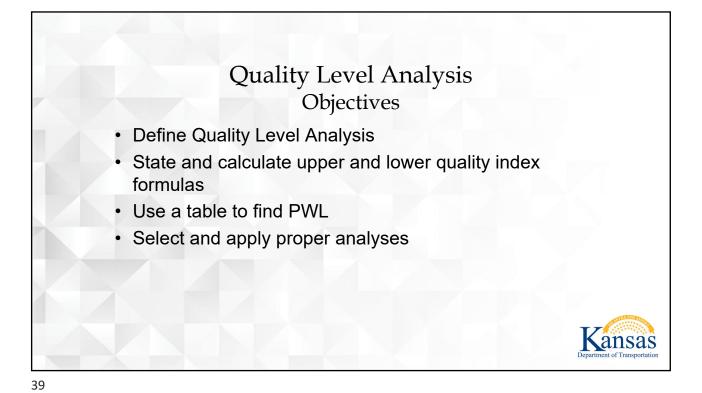


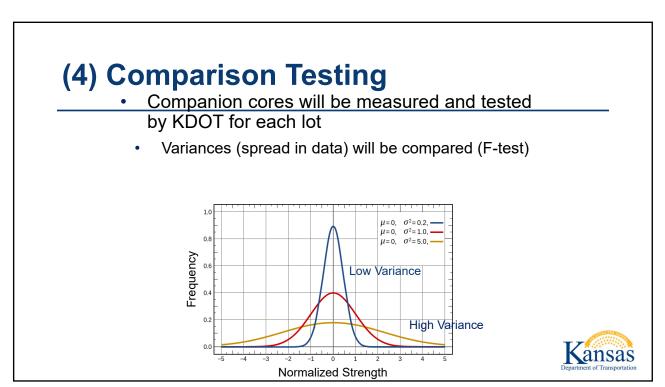
| | | | | Table | | iability U | Unknow | Percent V n Proced n Metho | lure | limits | | | | | |
|----------------------------------|------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------------------------|----------------|----------------|----------------|----------------|----------------|--------------|---------------|
| Quality | | | | | | | | | | | | | | n = 5 | |
| Index | | | | | rcent Wit | | | | | | | | | | |
| Q _U or Q _L | <u>N=3</u> | <u>N=4</u> | <u>N=5</u> | <u>N=6</u> | <u>N=7</u> | <u>N=8</u> | <u>N=9</u> | <u>N=10</u> | <u>N=15</u> | <u>N=20</u> | <u>N=30</u> | <u>N=50</u> | <u>N=100</u> | $Q_L = 1.25$ | |
| 1.00 | 83.33 | 83.33 | 83.64 | 83.80 | 83.90 | 83.96 | 84.00 | 84.03 | 84.09 | 84.11 | 84.12 | 84.13 | 84.13 | •1 | |
| 1.01 | 83.89 | 83.67 | 83.93 | 84.08 | 84.17 | 84.22 | 84.26 | 84.28 | 84.34 | 84.36 | 84.37 | 84.37 | 84.38 | | |
| 1.02 | 84.47 | 84.00 | 84.22 | 84.36 | 84.44 | 84.49 | 84.52 | 84.54 | 84.59 | 84.60 | 84.61 | 84.62 | 84.62 | DIAZI = 0.0 | E 4 |
| 1.03 | 85.07 | 84.33 | 84.52 | 84.63 | 84.70 | 84.75 | 84.77 | 84.79 | 84.83 | 84.85 | 84.85 | 84.85 | 84.85 | $PWL_L = 90$ | .34 |
| 1.04 | 85.69 | 84.67 | 84.81 | 84.91 | 84.97 | 85.00 | 85.03 | 85.04 | 85.08 | 85.09 | 85.09 | 85.09 | 85.09 | | |
| 1.05 | 86.34 | 85.00 | 85.09 | 85.18 | 85.23 | 85.26 | 85.28 | 85.29 | 85.32 | 85.33 | 85.33 | 85.32 | 85.32 | | |
| 1.00 | 5 87.02 | 85.33 | 85.38 | 85.45 | 85.49 | 85.51 | 85.53 | 85.54 | 85.56 | 85.56 | 85.56 | 85.55 | 85.55 | | |
| 1.07 | 87.73 | 85.67 | 85.67 | 85.71 | 85.74 | 85.76 | 85.78 | 85.78 | 85.80 | 85.80 | 85.79 | 85.78 | 85.78 | | |
| 1.08 | | 86.00 | 85.95 | 85.98 | 86.00 | 86.01 | 86.02 | 86.03 | 86.03 | 86.03 | 86.02 | 86.01 | 86.00 | | |
| 1.09 | | 86.33 | 86.24 | 86.24 | 86.25 | 86.26 | 86.27 | 86.27 | 86.26 | 86.26 | 86.25 | 86.23 | 86.23 | | |
| 1.10 | | 86.67 | 86.52 | 86.50 | 86.51 | 86.51 | 86.51 | 86.50 | 86.49 | 86.48 | 86.47 | 86.46 | 86.45 | | |
| 1.11 | | 87.00 | 86.80 | 86.76 | 86.75 | 86.75 | 86.74 | 86.74 | 86.72 | 86.71 | 86.69 | 86.68 | 86.66 | | |
| 1.12 | | 87.33 | 87.07 | 87.02 | 87.00 | 86.99 | 86.98 | 86.97 | 86.95 | 86.93 | 86.91 | 86.89 | 86.88 | | |
| 1.13 | | 87.67 | 87.35 | 87.28 | 87.25 | 87.23 | 87.21 | 87.20 | 87.17 | 87.15 | 87.13 | 87.11 | 87.09 | | |
| 1.14 | | 88.00 88.33 | 87.63 87.90 | 87.53 87.78 | 87.49 87.73 | 87.46 87.70 | 87.45 87.68 | 87.43 87.66 | 87.39 87.61 | 87.37 87.58 | 87.34 87.55 | 87.32 87.53 | 87.30 87.51 | | |
| 1.15 | | 88.67 | 88.17 | 87.78 | 87.75 | 87.93 | 87.08 | 87.88 | 87.82 | 87.78 | 87.76 | 87.55 | 87.51 | | |
| 1.16 | | 89.00 | 88.44 | 88.28 | 87.97 | 87.95 | 88.13 | 88.10 | 88.04 | 88.00 | 87.97 | 87.94 | 87.92 | | |
| 1.18 | | 89.33 | 88.71 | 88.53 | 88.44 | 88.39 | 88.35 | 88.32 | 88.25 | 88.21 | 88.18 | 88.15 | 88.12 | | |
| 1.19 | | 89.67 | 88.98 | 88.77 | 88.67 | 88.61 | 88.57 | 88.54 | 88.46 | | 88.38 | 88.35 | 88.32 | | |
| 1.20 | | 90.00 | 89.24 | 89.01 | 88.90 | 88.83 | 88.79 | 88.76 | 88.66 | 88.62 | 88.58 | 88.54 | 88.52 | | |
| 1.21 | | 90.33 | 89.50 | 89.25 | 89.13 | 89.06 | 89.00 | 88.97 | 88.87 | 88.82 | 88.78 | 88.74 | 88.71 | | |
| 1.22 | | 90.67 | 89.77 | 89.49 | 89.35 | 89.27 | 89.22 | 89.18 | | 89.02 | 88.97 | 88.93 | 88.91 | | STRA PER A |
| 1.23 | 1 | 91.00 | 90.03 | 89.72 | 89.58 | 89.49 | 89.43 | 89.39 | 89.27 | 89.22 | 89.16 | 89.12 | 89.09 | TZ | 10 |
| 1.24 | 100.00 | 91.33 | 90.28 | 89.96 | 89.80 | 89.70 | 89.64 | 89.59 | 89.47 | 89.41 | 89.36 | 89.31 | 89.28 | K | inc |
| (1.25 | 100.00 | 91.67 | 90.54 | 90.19 | 90.02 | 89.91 | 89.85 | 89.79 | 89.66 | 89.60 | 89.54 | 89.50 | 89.47 | | 11120 |
| 1.20 | 5 100.00 | 92.00 | 90.79 | 90.42 | 90.23 | 90.12 | 90.05 | 90.00 | 89.85 | 89.79 | 89.73 | 89.68 | 89.65 | Departmen | nt of Transpo |

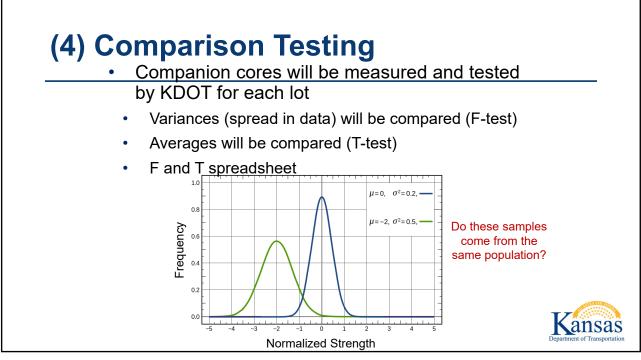


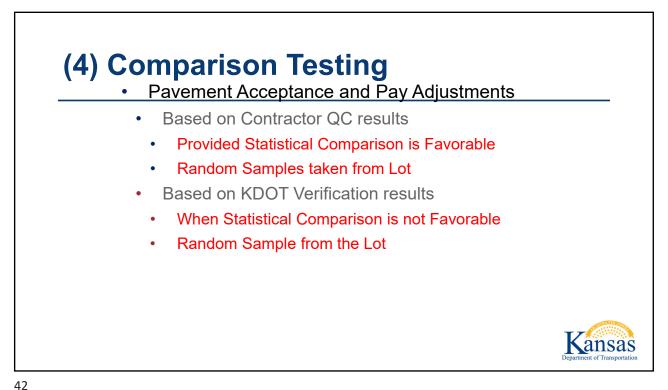


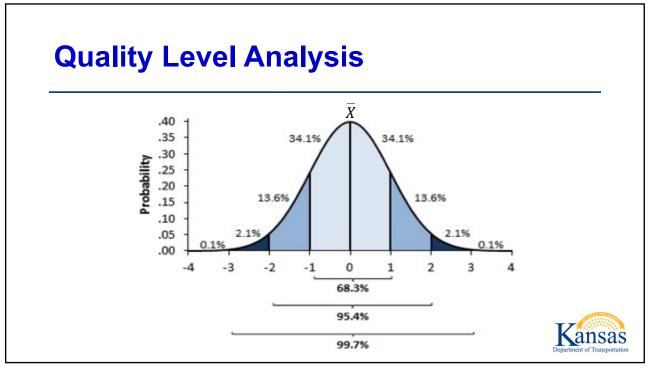
| 2 | | | | Table | Vari | iability U | Inknow | Percent V n Proced n Metho | | imits | | | | |
|----------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------------------------|----------------|----------------|----------------|----------------|----------------|------------------------------|
| Quality | | | | | | | | | | | | | | n = 5 |
| Index | NL 2 | NA | NL F | | | | | | mple Siz | | NL 20 | N 50 | N. 100 | |
| QU or QL | <u>N=3</u> | <u>N=4</u> | <u>N=5</u> | <u>N=6</u> | <u>N=7</u> | <u>N=8</u> | <u>N=9</u> | <u>N=10</u> | <u>N=15</u> | <u>N=20</u> | <u>N=30</u> | <u>N=50</u> | N=100 | $Q_L = 0.00$ |
| 0.00 | 50.00 | 50.00 | 50.00 | 50.00 | 50.00 | 50.00 | 50.00 | 50.00 | 50.00 | 50.00 | 50.00 | 50.00 | 50.00 | $Q_L = 0.00$ |
| 0.01 | 50.28 | 50.33 | 50.36 | 50.37 | 50.37 | 50.38 | 50.38 | 50.38 | 50.39 | 50.39 | 50.40 | 50.40 | 50.40 | |
| 0.02 | 50.55 | 50.67 | 50.71 | 50.73 | 50.75 | 50.76 | 50.76 | 50.77 | 50.78 | 50.79 | 50.79 | 50.79 | 50.80 | |
| 0.03 | 50.83 | 51.00 | 51.07 | 51.10 | 51.12 | 51.14 | 51.15 | 51.15 | 51.17 | 51.18 | 51.19 | 51.19 | 51.19 | $PWL_{L} = 50.00$ |
| 0.04 | 51.10 | 51.33 | 51.42 | 51.47 | 51.50 | 51.51 | 51.53 | 51.54 | 51.56 | 51.57 | 51.58 | 51.59 | 51.59 | $I V L_{L} = 30.00$ |
| 0.05 | 51.38 | 51.67 | 51.78 | 51.84 | 51.87 | 51.89 | 51.91 | 51.92 | 51.95 | 51.96 | 51.98 | 51.98 | 51.99 | |
| 0.06 | 51.65 | 52.00 | 52.13 | 52.20 | 52.24 | 52.27 | 52.29 | 52.30 | 52.34 | 52.36 | 52.37 | 52.38 | 52.39 | |
| 0.07 | 51.93 | 52.33 | 52.49 | 52.57 52.94 | 52.62 52.99 | 52.65 | 52.67 53.05 | 52.69 | 52.73 53.12 | 52.75 53.14 | 52.76 53.16 | 52.78 53.17 | 52.78 | |
| 0.08 | 52.21 52.48 | 52.67 53.00 | 52.85 53.20 | 53.30 | 53.37 | 53.03 53.41 | 53.43 | 53.07 53.46 | 53.12 | 53.53 | 53.10 | 53.57 | 53.18 53.58 | |
| 0.09 | 52.46 | 53.33 | 53.56 | 53.67 | 53.74 | 53.78 | 53.82 | 53.40 | 53.90 | 53.92 | 53.95 | 53.96 | 53.97 | |
| 0.11 | 53.04 | 53.67 | 53.91 | 54.04 | 54.11 | 54.16 | 54.20 | 54.22 | 54.29 | 54.31 | 54.34 | 54.36 | 54.37 | |
| 0.12 | 53.31 | 54.00 | 54.27 | 54.40 | 54.49 | 54.54 | 54.58 | 54.60 | 54.67 | 54.70 | 54.73 | 54.75 | 54.76 | |
| 0.13 | 53.59 | 54.33 | 54.62 | 54.77 | 54.86 | 54.92 | 54.96 | 54.99 | 55.06 | 55.09 | 55.12 | 55.14 | 55.16 | |
| 0.14 | 53.87 | 54.67 | 54.98 | 55.14 | 55.23 | 55.29 | 55.34 | 55.37 | 55.45 | 55.48 | 55.52 | 55.54 | 55.55 | |
| 0.15 | 54.15 | 55.00 | 55.33 | 55.50 | 55.60 | 55.67 | 55.71 | 55.75 | 55.84 | 55.87 | 55.91 | 55.93 | 55.95 | |
| 0.16 | 54.42 | 55.33 | 55.69 | 55.87 | 55.97 | 56.04 | 56.09 | 56.13 | 56.22 | 56.26 | 56.30 | 56.32 | 56.34 | |
| 0.17 | 54.70 | 55.67 | 56.04 | 56.23 | 56.35 | 56.42 | 56.47 | 56.51 | 56.61 | 56.65 | 56.69 | 56.71 | 56.73 | |
| 0.18 | 54.98 | 56.00 | 56.40 | 56.60 | 56.72 | 56.79 | 56.85 | 56.89 | 56.99 | 57.04 | 57.08 | 57.11 | 57.12 | |
| 0.19 | 55.26 | 56.33 56.67 | 56.75 57.10 | 56.96 57.32 | 57.09 57.46 | 57.17 57.54 | 57.23 57.60 | 57.27 57.65 | 57.38 57.76 | 57.43 57.81 | 57.47 57.85 | 57.50 57.89 | 57.52 57.91 | |
| 0.20 | 55.54 55.82 | 57.00 | 57.46 | 57.69 | 57.83 | 57.92 | 57.98 | 58.03 | 58.15 | 57.81 | 57.85 | 57.89 | 57.91 | |
| 0.21 | 56.10 | 57.33 | 57.81 | 58.05 | 58.20 | 58.29 | 58.36 | 58.40 | 58.53 | 58.58 | 58.63 | 58.66 | 58.69 | |
| 0.23 | 56.38 | 57.67 | 58.16 | 58.41 | 58.56 | 58.66 | 58.73 | 58.78 | 58.91 | 58.97 | 59.01 | 59.05 | 59.07 | |
| 0.24 | 56.66 | 58.00 | 58.52 | 58.78 | 58.93 | 59.03 | 59.11 | 59.16 | 59.29 | 59.35 | 59.40 | 59.44 | 59.46 | A STATISTICS |
| 0.25 | 56.95 | 58.33 | 58.87 | 59.14 | 59.30 | 59.41 | 59.48 | 59.53 | 59.67 | 59.73 | 59.78 | 59.82 | 59.85 | |
| 0.26 | 57.23 | 58.67 | 59.22 | 59.50 | 59.67 | 59.78 | 59.85 | 59.91 | 60.05 | 60.11 | 60.17 | 60.21 | 60.23 | Kansas |
| 0.27 | 57.51 | 59.00 | 59.57 | 59.86 | 60.03 | 60.15 | 60.23 | 60.28 | 60.43 | 60.49 | 60.55 | 60.59 | 60.62 | INalisas |
| 0.28 | 57.80 | 59.33 | 59.92 | 60.22 | 60.40 | 60.52 | 60.60 | 60.66 | 60.81 | 60.87 | 60.93 | 60.97 | 61.00 | Department of Transportation |
| 0.29 | 58.08 | 59.67 | 60.28 | 60.58 | 60.77 | 60.89 | 60.97 | 61.03 | 61.19 | 61.25 | 61.31 | 61.35 | 61.38 | |

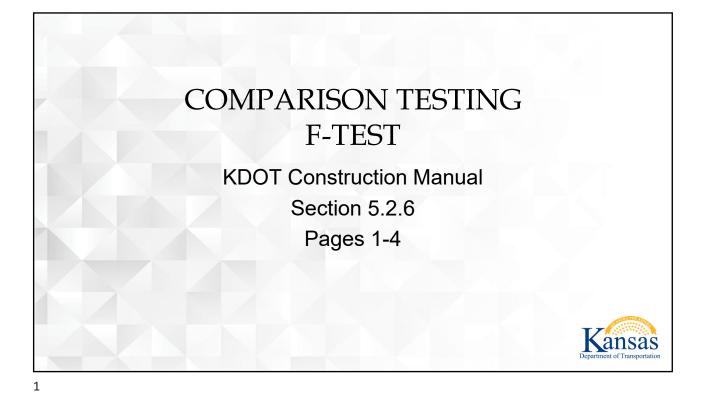


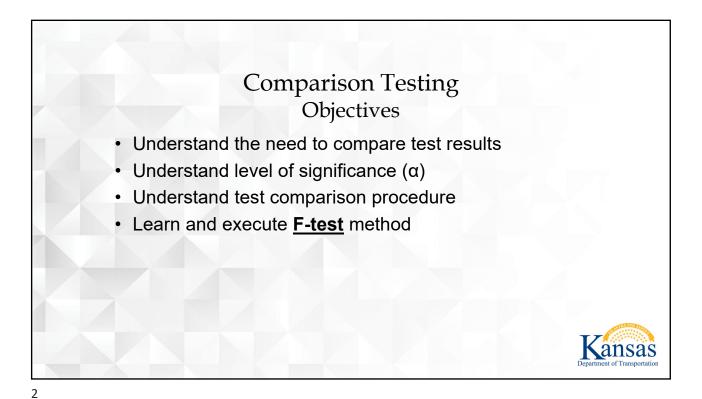


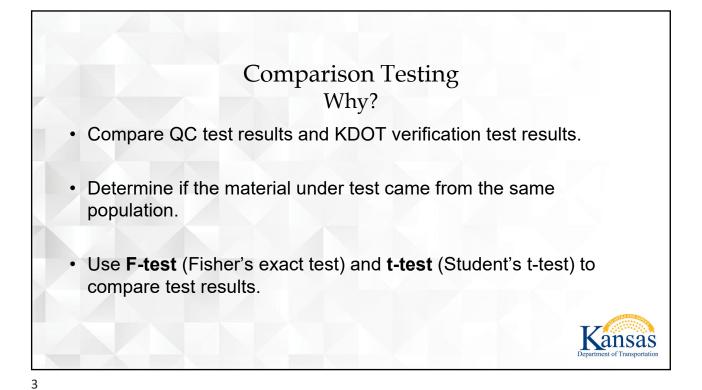


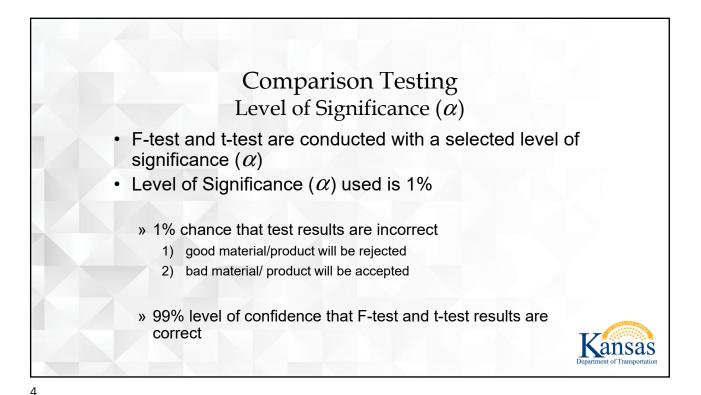


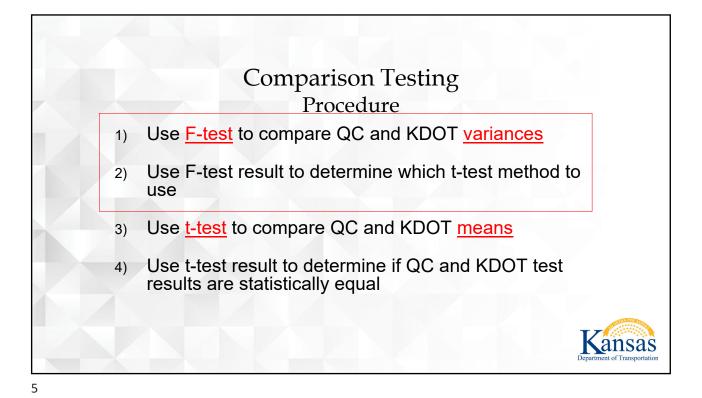




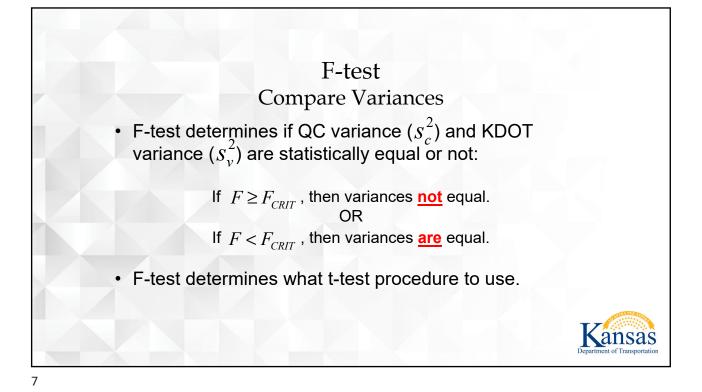


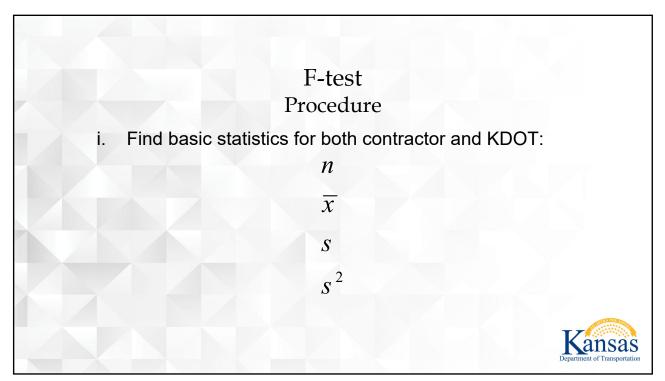


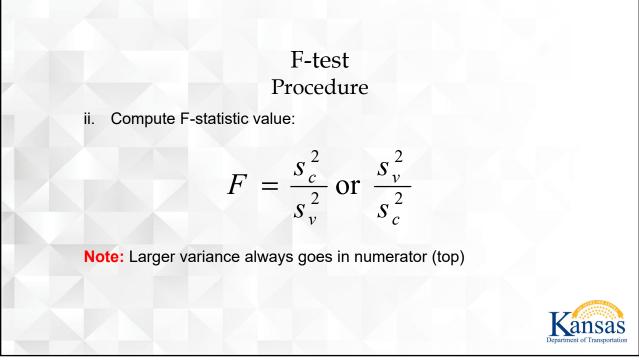




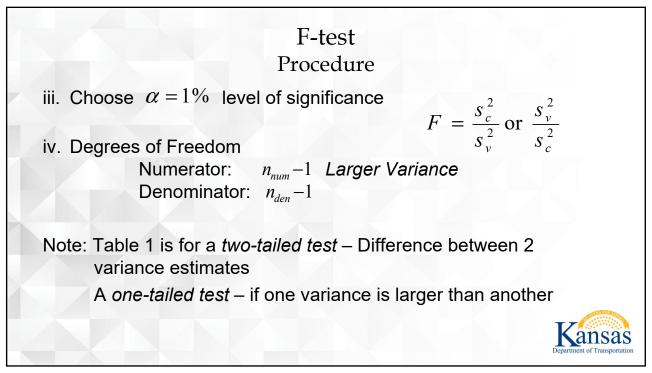






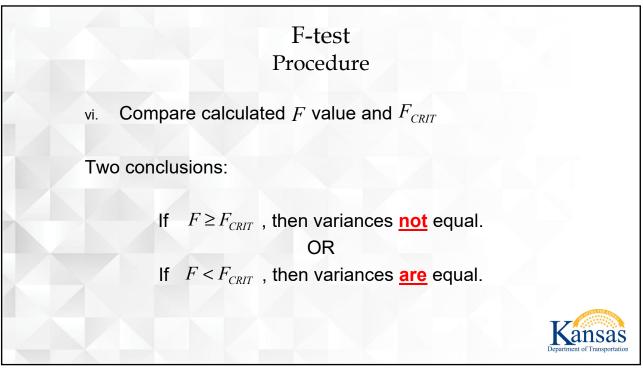


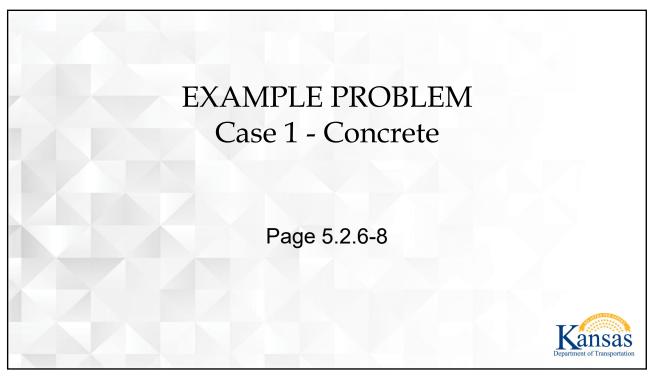


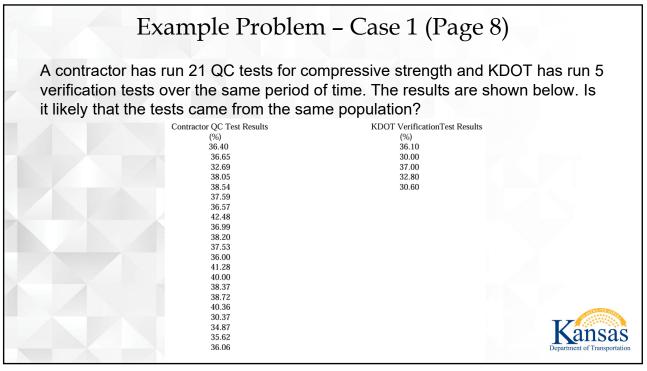


| | | | | F- | tes | t Pr | oceo | dure | ć | | | | |
|----------------------------|------|----------------------|--------------|--------------|--------------|---------------------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|
| V. | Find | F_{CP} | т İ | n Ta | ble ' | 1 (Pa | ades | 3-4 |) | | | | |
| | | - CK | - | | | | | | / | | | | |
| | | Tabl | e 1 | C | ritical Val | ues, F _{crit} fo | r the F-tes | t for a Lev | el of Signi | ficance, a | =1% | | |
| | | | | DE | GREES OF I | FREEDOM F | OR NUMER | ATOR | | | | | |
| | | | | | | | | | | | | | |
| | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| r. | 1 | 16200 | 20000 | 21600 | 22500 | 23100 | 23400 | 23700 | 23900 | 24100 | 24200 | 24300 | 24400 |
| õ | 2 | 198 | 199 | 199 | 199 | 199 | 199 | 199 | 199 | 199 | 199 | 199 | 199 |
| TA1 | 3 | 55.6 | 49.8 | 47.5 | 46.2 | 45.4 | 44.8 | 44.4 | 44.1 | 43.9 | 43.7 | 43.5 | 43.4 |
| ų. | 4 | 31.3 | 26.3 | 24.3 | 23.2 | 22.5 | 22.0 | 21.6 | 21.4 | 21.1 | 21.0 | 20.8 | 20.7 |
| NO | 5 | 22.8 | 18.3 | 16.5 | 15.6 | 14.9 | 14.5 | 14.2 | 14.0 | 13.8 | 13.6 | 13.5 | 13.4 |
| EN | 6 | 18.6 | 14.5 | 12.9 | 12.0 | 11.5 | 11.1 | 10.8 | 10.6 | 10.4 | 10.2 | 10.1 | 10.0 |
| 2 | 7 | 16.2 | 12.4 | 10.9 | 10.0 | 9.52 | 9.16 | 8.89 | 8.68 | 8.51 | 8.38 | 8.27 | 8.18 |
| IO. | 8 | 14.7 | 11.0 | 9.60 | 8.81 | 8.30 | 7.95 | 7.69 | 7.50 | 7.34 | 7.21 | 7.10 | 7.01 |
| N N | 9 | 13.6 | 10.1 | 8.72 | 7.96 | 7.47 | 7.13 | 6.88 | 6.69 | 6.54 | 6.42 | 6.31 | 6.23 |
| 0 | 10 | 12.8 | 9.43 8.91 | 8.08 7.60 | 7.34 6.88 | 6.87 6.42 | 6.54 6.10 | 6.30 5.86 | 6.12 5.68 | 5.97 5.54 | 5.85 5.42 | 5.75 5.32 | 5.66 5.24 |
| EE | 11 | 12.2 | 8.91 | 7.60 | 6.88 | 6.42 | 6.10 5.76 | 5.86 | 5.68 | 5.54 | 5.42 | 5.32 | 5.24 |
| OF FREEDOM FOR DENOMINATOR | 12 | 11.8 | 7.70 | 6.48 | 5.80 | 5.37 | 5.07 | 4.85 | 4.67 | 4.54 | 4.42 | 4.99 | 4.91 |
| OF 1 | 20 | 9.94 | 6.99 | 5.82 | 5.17 | 4.76 | 4.47 | 4.85 | 4.07 | 3.96 | 3.85 | 4.33 | 3.68 |
| SC | 20 | 9.55 | 6.66 | 5.52 | 4.89 | 4.49 | 4.47 | 3.99 | 3.83 | 3.69 | 3.59 | 3.50 | 3.42 |
| DEGREES | 30 | 9.18 | 6.35 | 5.24 | 4.62 | 4.23 | 3.95 | 3.74 | 3.58 | 3.45 | 3.34 | 3.25 | 3.18 |
| GR | 40 | 8.83 | 6.07 | 4.98 | 4.37 | 3.99 | 3.71 | 3.51 | 3.35 | 3.22 | 3.12 | 3.03 | 2.95 |
| DE | 60 | 8.49 | 5.80 | 4.73 | 4.14 | 3.76 | 3.49 | 3.29 | 3.13 | 3.01 | 2.90 | 2.82 | 2.74 |
| | 120 | 8.18 | 5.54 | 4.50 | 3.92 | 3.55 | 3.28 | 3.09 | 2.93 | 2.81 | 2.71 | 2.62 | 2.54 |
| | 20 | 7.88 | 5.30 | 4.28 | 3.72 | 3.35 | 3.09 | 2.90 | 2.74 | 2.62 | 2.52 | 2.43 | 2.34 |
| | | or a <i>two-tail</i> | | | | | | | | 2.08 | 2.00 | | 2.00 |

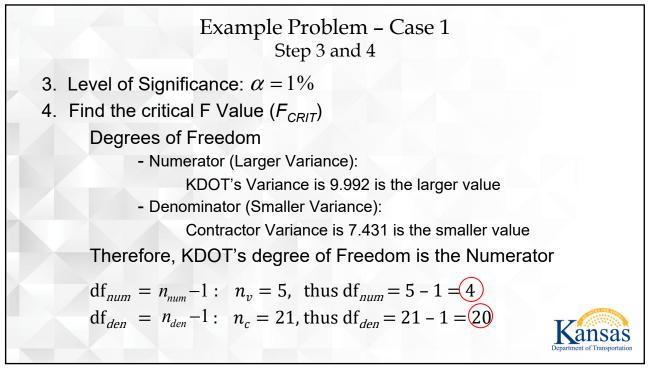
| | | | | D | EGREES OF | FREEDOM | FOR NUME | RATOR | | | | | |
|--------|-------------|-----------------------|--------------|-------------|-------------|--------------------------|------------|-------|-------|-------|-------|-------|-------|
| | | | | | | | | | | | | | |
| | | 15 | 20 | 24 | 30 | 40 | 50 | 60 | 100 | 120 | 200 | 500 | œ |
| | 1 | 24600 | 24800 | 24900 | 25000 | 25100 | 25200 | 25300 | 25300 | 25400 | 25400 | 25400 | 25500 |
| | 2 | 199 | 199 | 199 | 199 | 199 | 199 | 199 | 199 | 199 | 199 | 199 | 200 |
| | 3 | 43.1 | 42.8 | 42.69 | 42.5 | 42.3 | 42.2 | 42.1 | 42.0 | 42.0 | 41.9 | 41.9 | 41.8 |
| | 4 | 20.4 | 20.2 | 20.0 | 19.9 | 19.8 | 19.7 | 19.6 | 19.5 | 19.5 | 19.4 | 19.4 | 19.3 |
| | 5 | 13.1 | 12.9 | 12.8 | 12.7 | 12.5 | 12.5 | 12.4 | 12.3 | 12.3 | 12.2 | 12.2 | 12.1 |
| | 6 | 9.81 | 9.59 | 9.47 | 9.36 | 9.24 | 9.17 | 9.12 | 9.03 | 9.00 | 8.95 | 8.91 | 8.88 |
| | 7 | 7.97 | 7.75 | 7.65 | 7.53 | 7.42 | 7.35 | 7.31 | 7.22 | 7.19 | 7.15 | 7.10 | 7.08 |
| | 8 | 6.81 | 6.61 | 6.50 | 6.40 | 6.29 | 6.22 | 6.18 | 6.09 | 6.06 | 6.02 | 5.98 | 5.95 |
| | 9 | 6.03 | 5.83 | 5.73 | 5.62 | 5.52 | 5.45 | 5.41 | 5.32 | 5.30 | 5.26 | 5.21 | 5.19 |
| | 10 | 5.47 | 5.27 | 5.17 | 5.07 | 4.97 | 4.90 | 4.86 | 4.77 | 4.75 | 4.71 | 4.67 | 4.64 |
| | 11 | 5.05 | 4.86 | 4.76 | 4.65 | 4.55 | 4.49 | 4.45 | 4.36 | 4.34 | 4.29 | 4.25 | 4.23 |
| | 12 | 4.72 | 4.53 | 4.43 | 4.33 | 4.23 | 4.17 | 4.12 | 4.04 | 4.01 | 3.97 | 3.93 | 3.90 |
| | 15 | 4.07 | 3.88 | 3.79 | 3.69 | 3.59 | 3.52 | 3.48 | 3.39 | 3.37 | 3.33 | 3.29 | 3.26 |
| | 20 | 3.50 | 3.32 | 3.22 | 3.12 | 3.02 | 2.96 | 2.92 | 2.83 | 2.81 | 2.76 | 2.72 | 2.69 |
| | 24 | 3.25 | 3.06 | 2.97 | 2.87 | 2.77 | 2.70 | 2.66 | 2.57 | 2.55 | 2.50 | 2.46 | 2.43 |
| | 30 | 3.01 | 2.82 | 2.73 | 2.63 | 2.52 | 2.46 | 2.42 | 2.32 | 2.30 | 2.25 | 2.21 | 2.18 |
| | 40 | 2.78 | 2.60 | 2.50 | 2.40 | 2.3 | 2.23 | 2.18 | 2.09 | 2.06 | 2.01 | 1.96 | 1.93 |
| | 60 | 2.57 | 2.39 | 2.29 | 2.19 | 2.08 | 2.01 | 1.96 | 1.86 | 1.83 | 1.78 | 1.73 | 1.69 |
| | 120 | 2.37 | 2.19 | 2.09 | 1.98 | 1.87 | 1.80 | 1.75 | 1.64 | 1.61 | 1.54 | 1.48 | 1.43 |
| | 00 | 2.19 | 2.00 | 1.90 | 1.79 | 1.67 | 1.59 | 1.53 | 1.40 | 1.36 | 1.28 | 1.17 | 1.00 |
| NOTE : | This is for | r a <i>two-tail</i> e | ed test with | the null an | d alternate | hypothese | s shown be | low: | | | | | |
| | | | | | | $H_o: s^2$ $H_a: s^2$ | 2 | | | | | | |

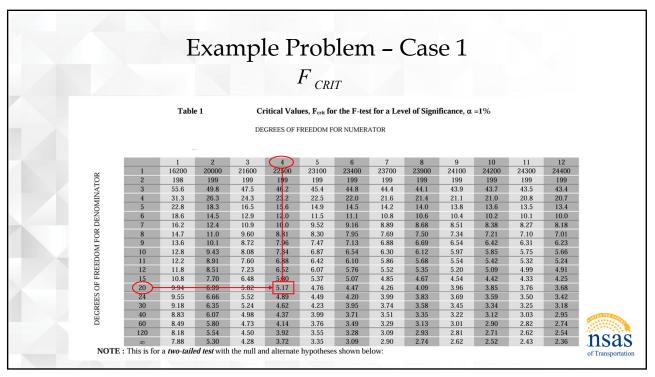


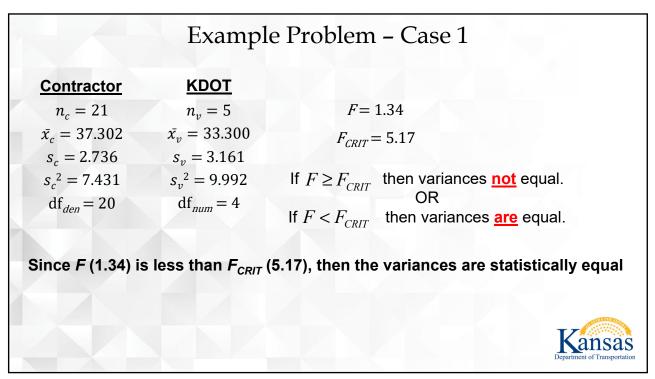


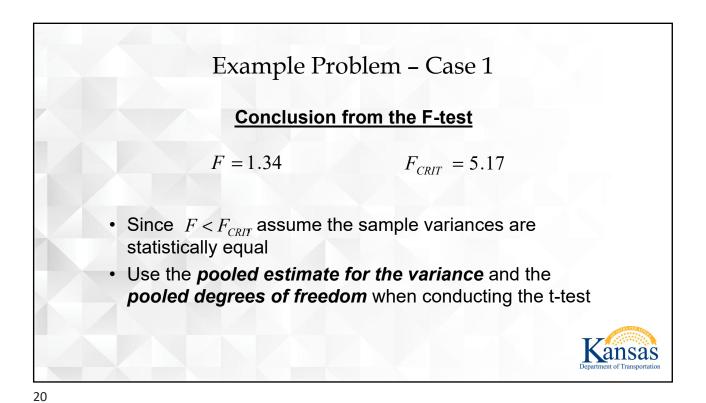


Example Problem – Case 1 Step 1: Compute the Statistics Contractor KDOT $n_{c} = 21$ $n_v = 5$ $\bar{x}_{c} = 37.302$ $\bar{x_v} = 33.300$ $s_c = 2.736$ $s_v = 3.161$ $s_c^2 = 7.431$ $s_v^2 = 9.992$ Step 2: Compute the F Statistic $F = \frac{s_c^2}{s_v^2} \operatorname{or} \left(\frac{s_v^2}{s_v^2} \right)$ $F = \frac{9.992}{7.431} = 1.34$ Note: Larger variance always goes in numerator (top) ansas

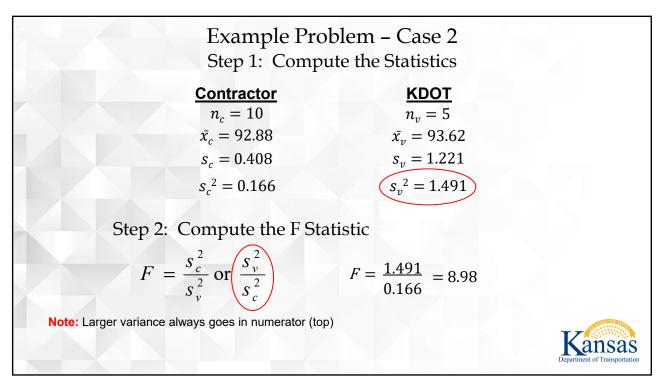


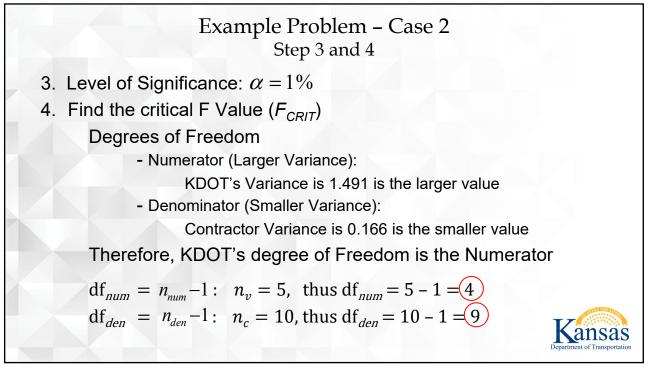


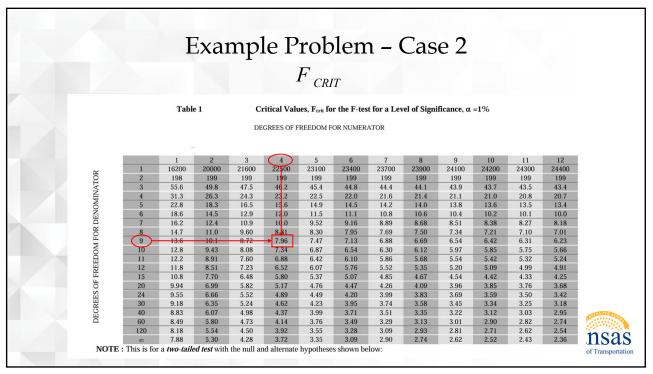


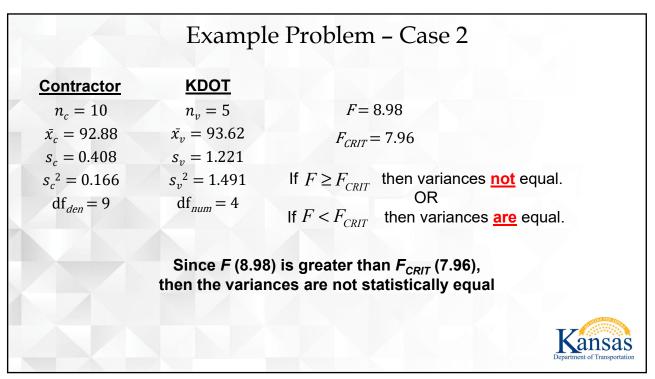


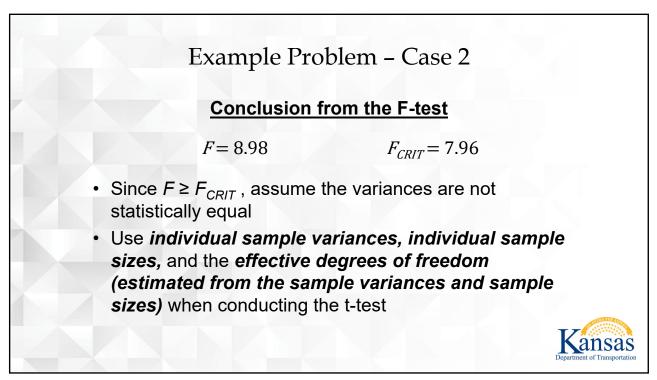
| | Example Proble | m – Case 2 (Page 10) | |
|---------|--|---|-----|
| same pe | eriod of time for the asphalt p | KDOT has run 5 verification tests over the avement density (%G _{mm}). The results are came from the same population or lot? | e |
| | Contractor QC Test Results 93.0 92.4 92.9 93.6 92.9 92.9 92.4 93.4 92.9 92.9 92.4 | KDOT Verification Test Results 95.5 93.3 94.1 92.5 92.7 | Sas |

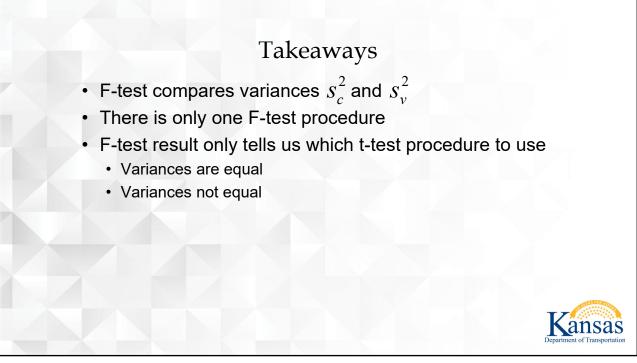


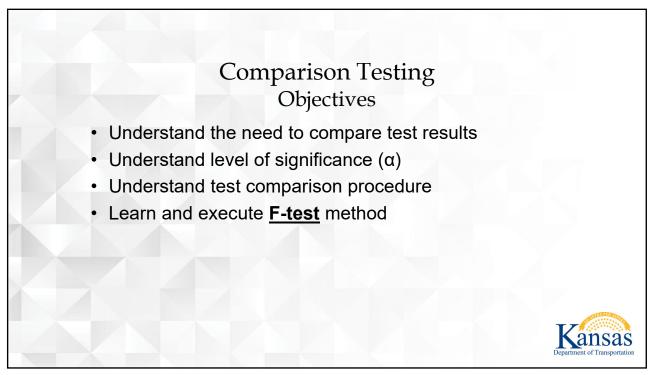


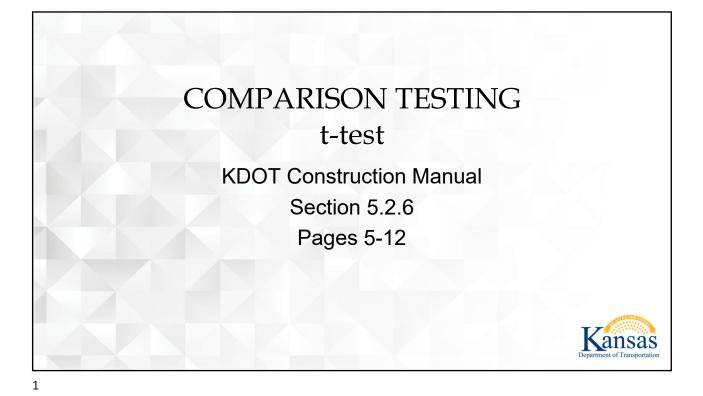


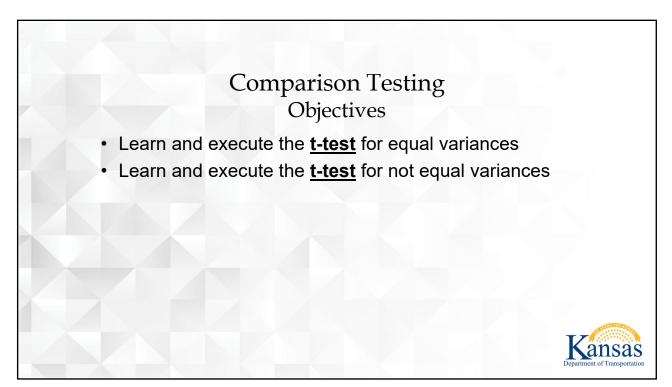


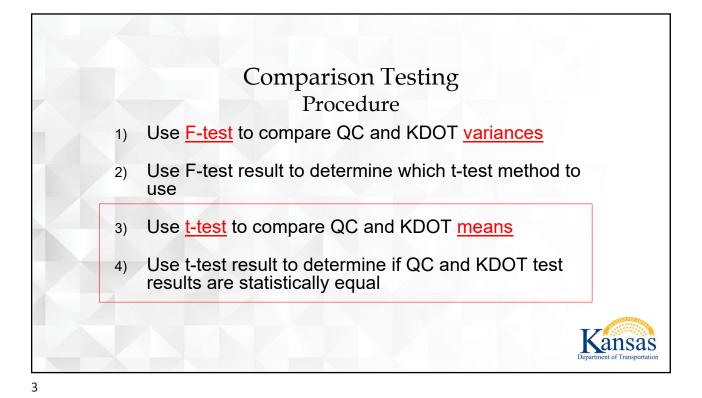


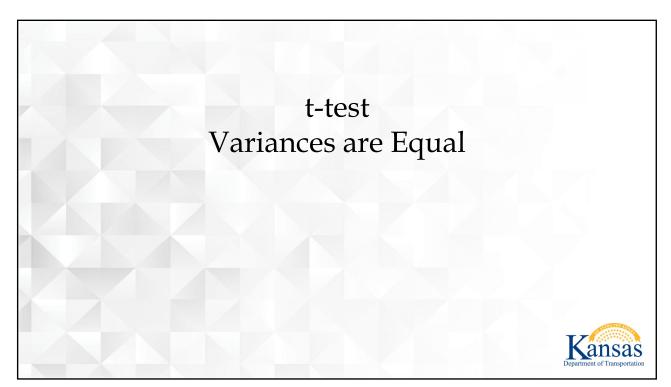


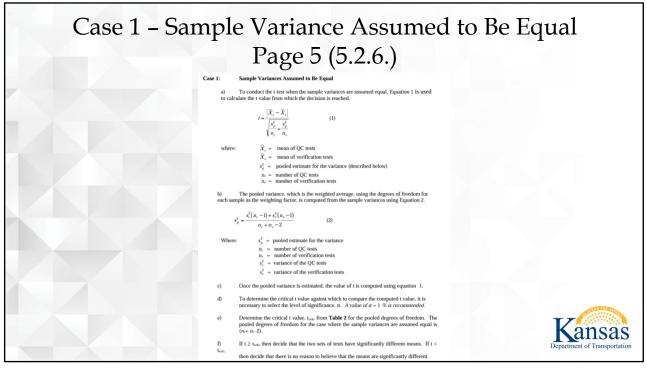


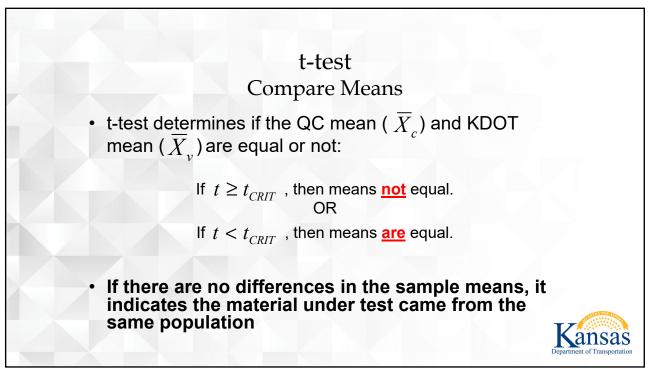


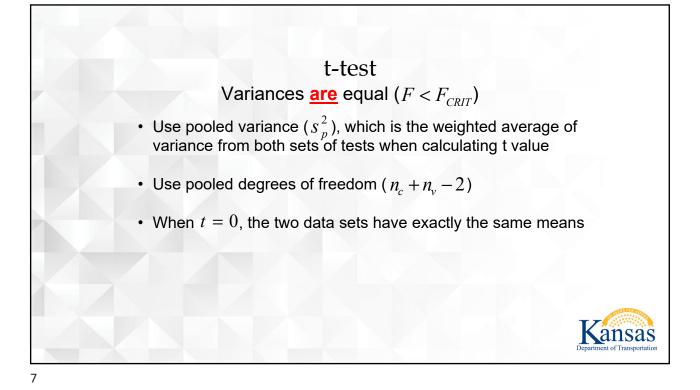


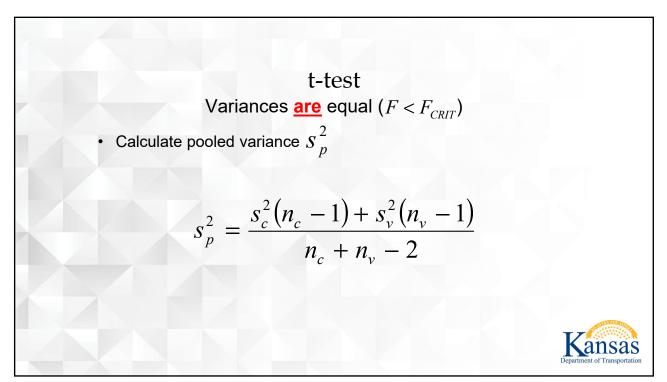


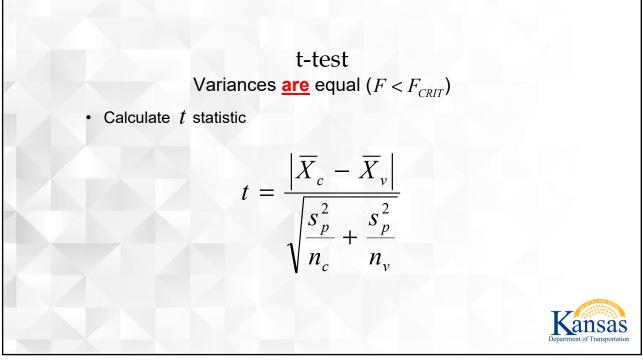




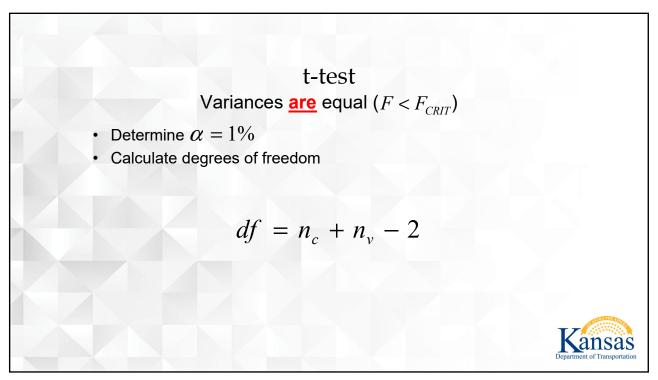


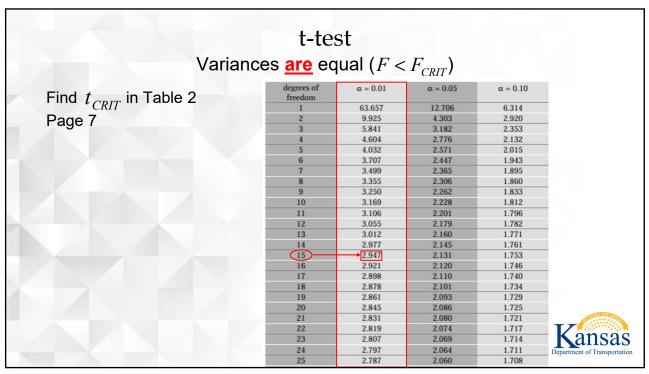


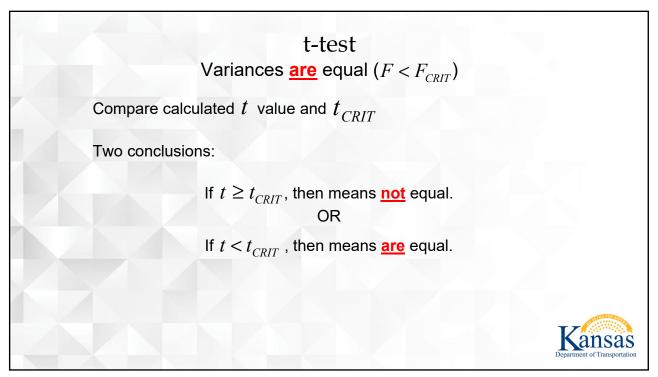


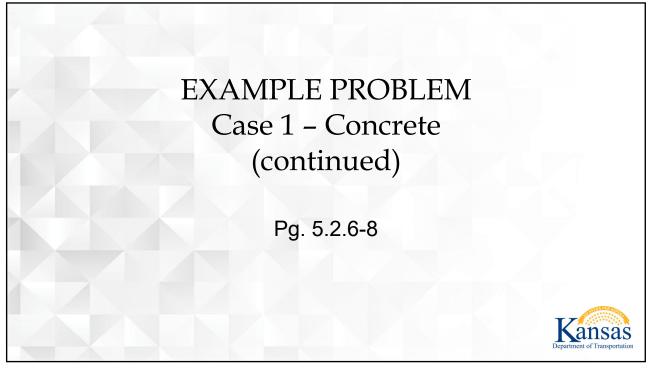


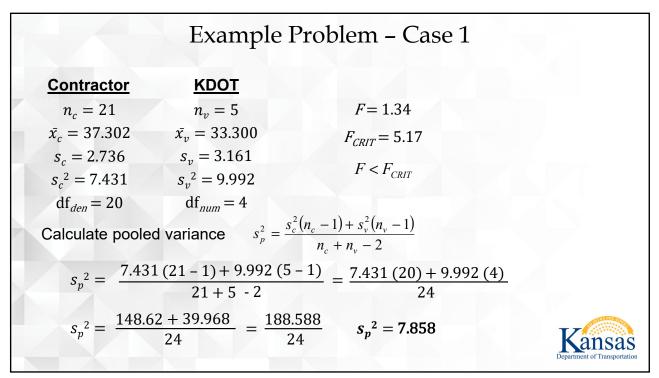


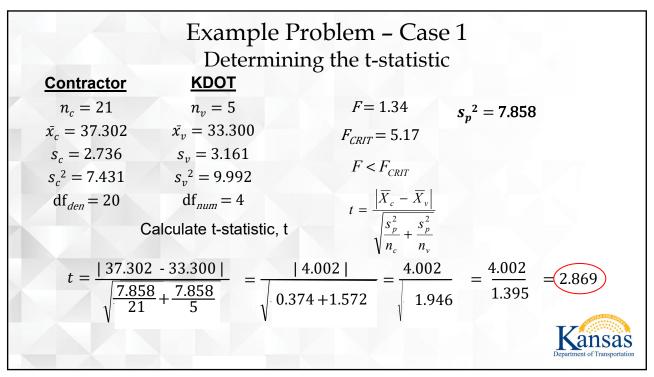




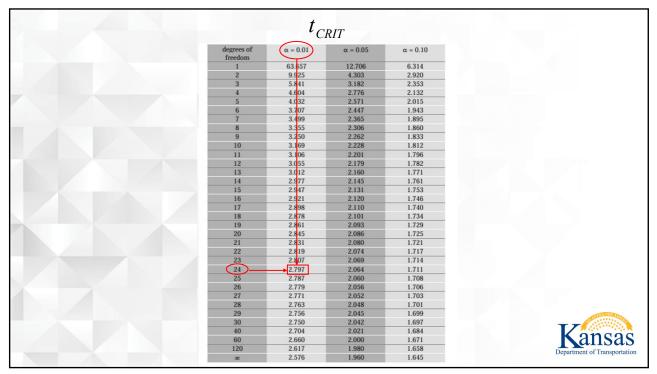


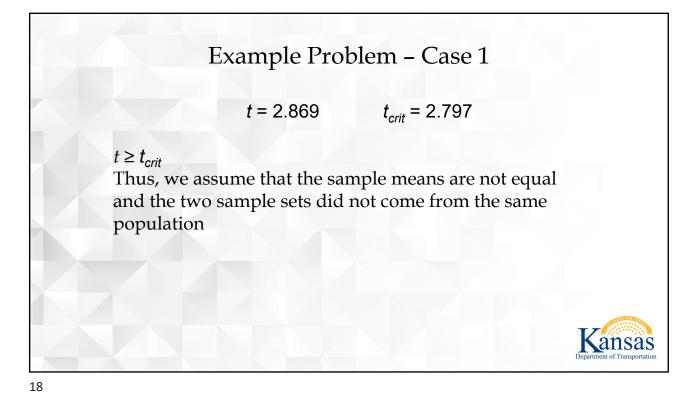


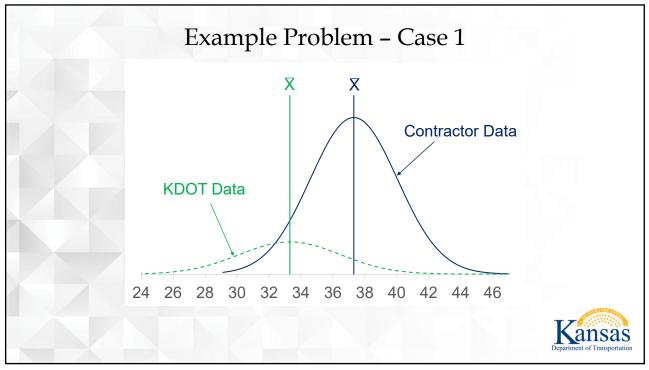


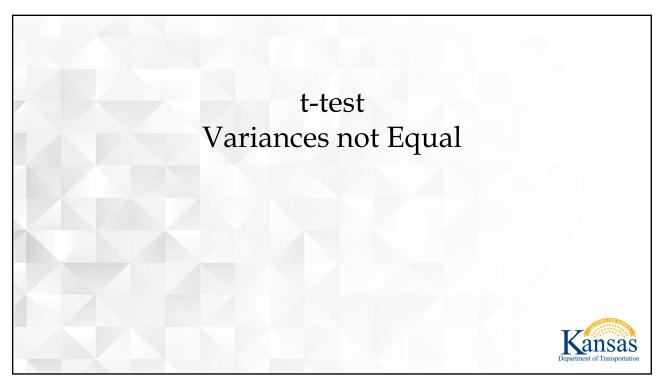


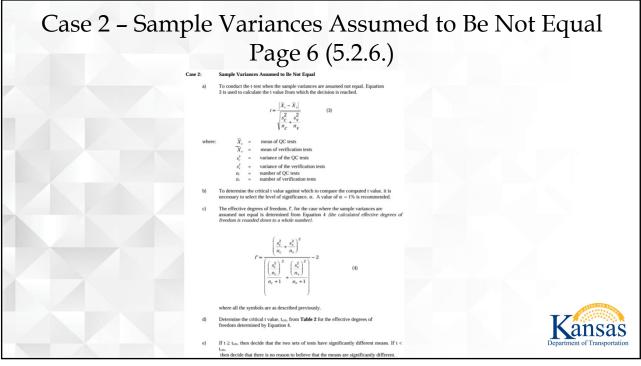
Example Problem – Case 1 Determining the t-statistic <u>KDOT</u> Contractor F = 1.34 $s_p^2 = 7.858$ $n_{c} = 21$ $n_{v} = 5$ $\bar{x}_c = 37.302$ $\bar{x_v} = 33.300$ $F_{CRIT} = 5.17$ t = 2.869 $s_c = 2.736$ $s_v = 3.161$ $F < F_{CRIT}$ $s_v^2 = 9.992$ $s_c^2 = 7.431$ $df_{den} = 20$ $df_{num} = 4$ Calculate critical t-value, tcrit Pooled Degrees of Freedom = $n_c + n_v - 2 = 21 + 5 - 2 = 24$ $\alpha = 1\%$ Enter Table 2 with the Pooled Degrees of Freedom and α ansas

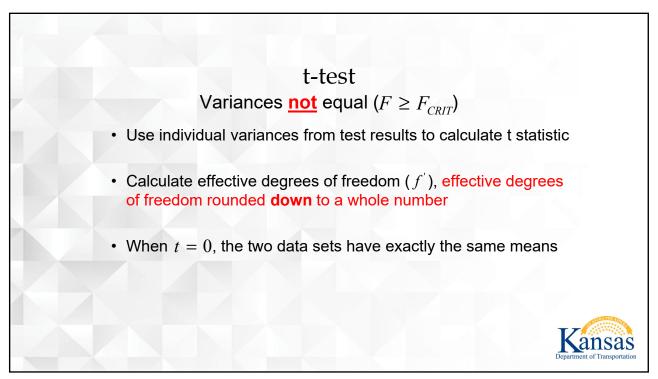


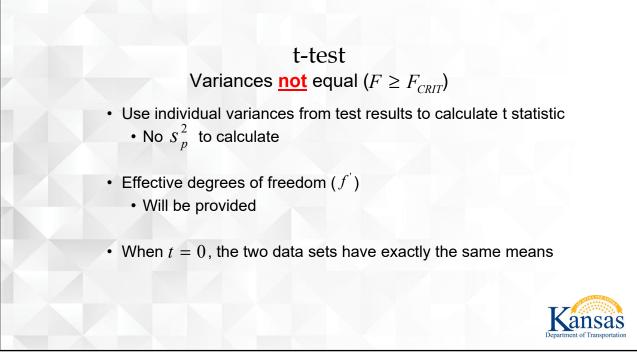


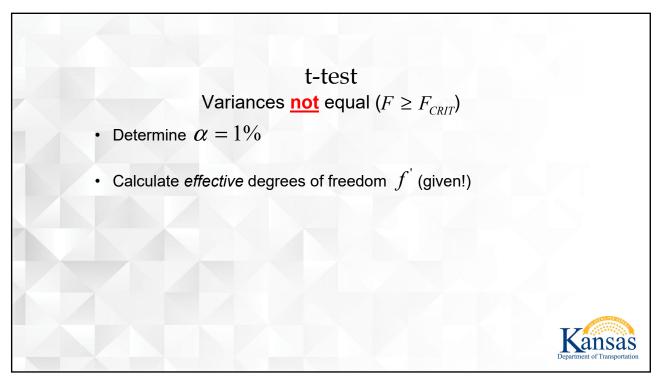


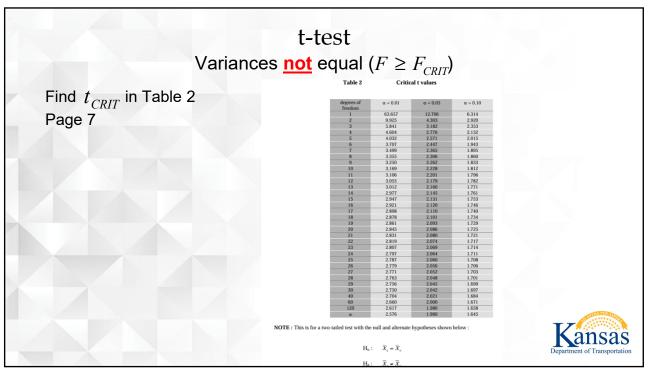


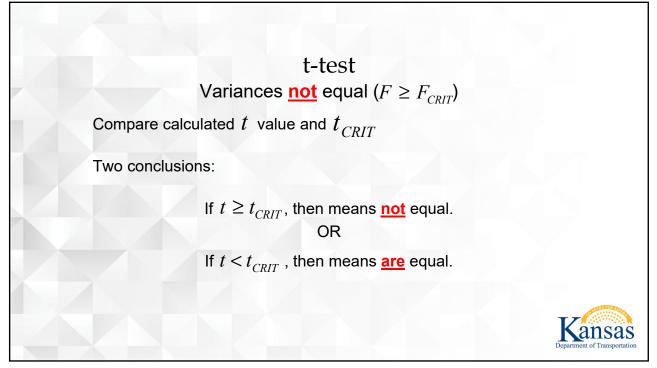


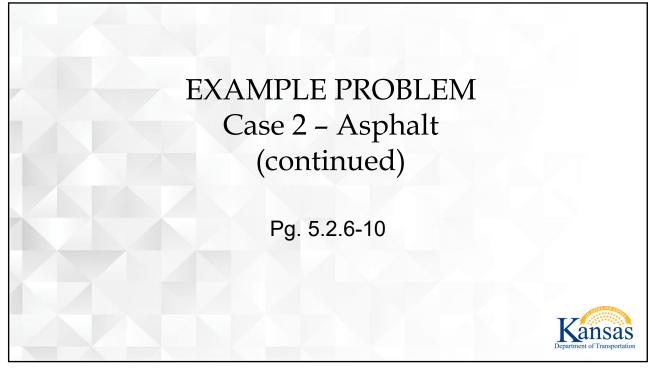


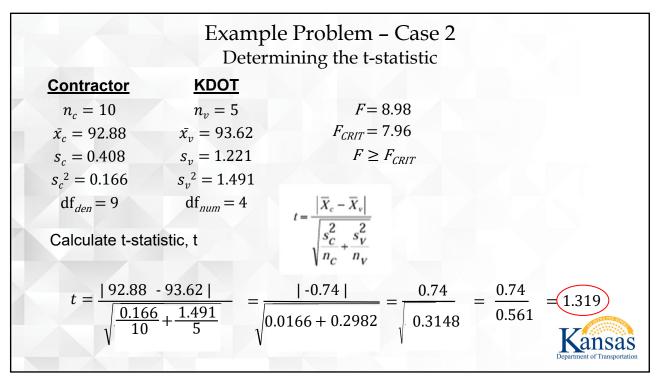


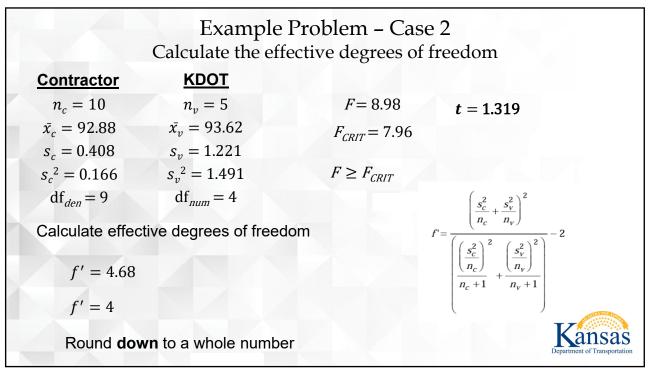


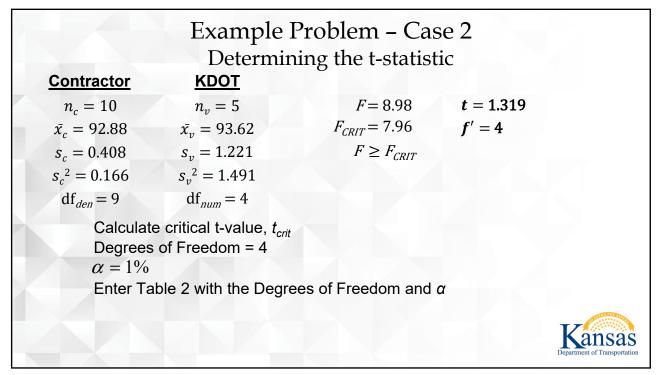




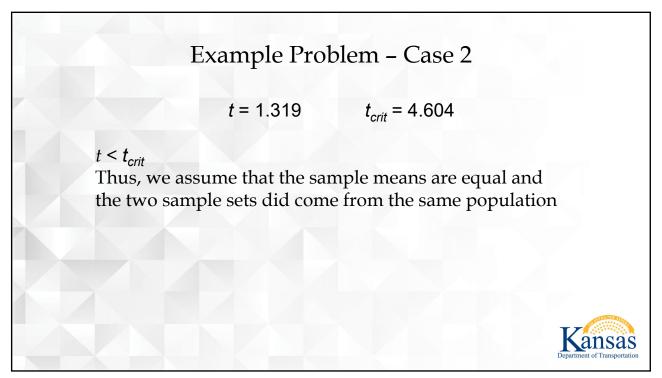


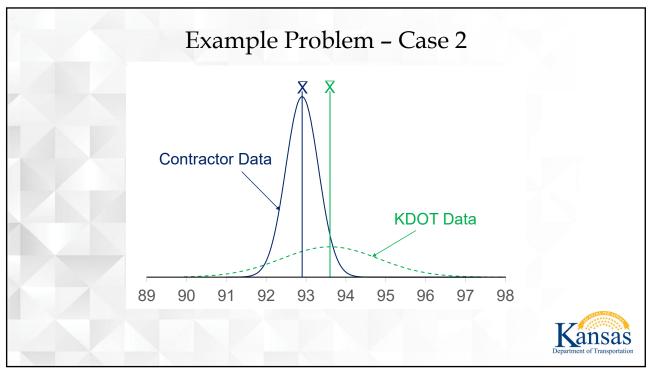


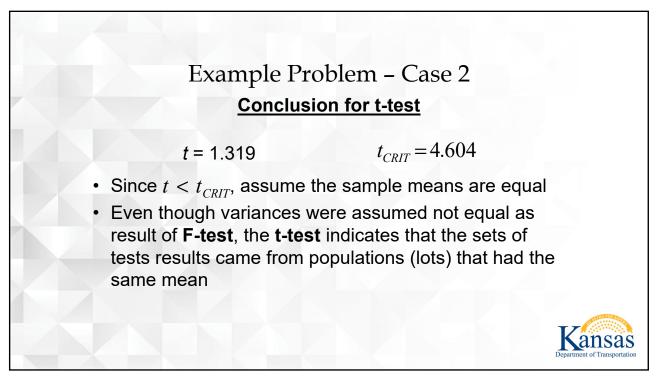


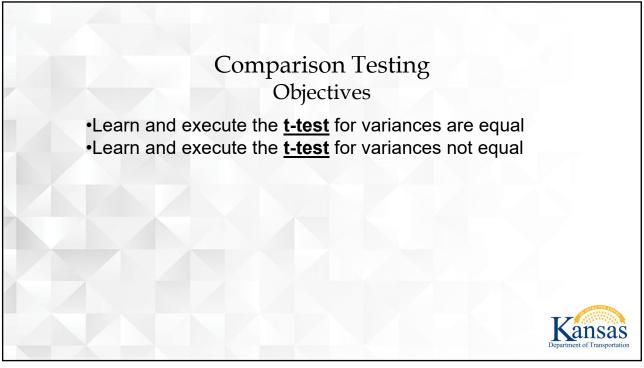


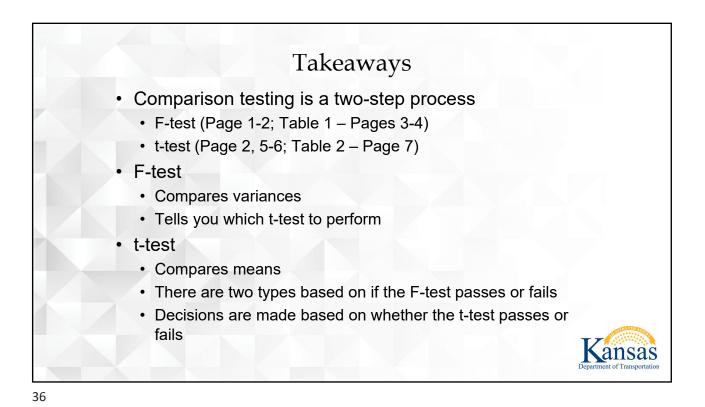
| | t_{C} | | | |
|-----------------------|-----------------------|----------|----------|----------|
| | ^{<i>v</i>} C | RIT | | |
| degrees of freedom | α = 0.01 | α = 0.05 | α = 0.10 | |
| 1 | 63.657 | 12.706 | 6.314 | |
| 2 | 9.925 | 4.303 | 2.920 | |
| 3 | 5.841 | 3.182 | 2.353 | |
| 4 | 4.604 | 2.776 | 2.132 | |
| 5 | 4.032 | 2.571 | 2.015 | |
| 6 | 3.707 | 2.447 | 1.943 | |
| 7 | 3.499 | 2.365 | 1.895 | |
| 8 | 3.355 | 2.306 | 1.860 | |
| 9 | 3.250 | 2.262 | 1.833 | |
| 10 | 3.169 | 2.228 | 1.812 | |
| 11 | 3.106 | 2.201 | 1.796 | |
| 12 | 3.055 | 2.179 | 1.782 | |
| 13 | 3.012 | 2.160 | 1.771 | |
| 13 | 2.977 | 2.145 | 1.761 | |
| 14 | 2.947 | 2.131 | 1.753 | |
| 15 | 2.921 | 2.120 | 1.746 | |
| 17 | 2.898 | 2.110 | 1.740 | |
| 17 | 2.898 | 2.101 | 1.740 | |
| 19 | 2.861 | 2.093 | 1.729 | |
| 20 | 2.861 | 2.086 | 1.725 | |
| 20 | 2.845 | 2.080 | 1.725 | |
| 21 22 | 2.831 | 2.080 | 1.721 | |
| 22 | 2.819 | 2.074 | 1.717 | |
| | | | | |
| 24 | 2.797 | 2.064 | 1.711 | |
| 25 | 2.787 | 2.060 | 1.708 | |
| 26 | 2.779 | 2.056 | 1.706 | |
| 27 | 2.771 | 2.052 | 1.703 | |
| 28 | 2.763 | 2.048 | 1.701 | |
| 29 | 2.756 | 2.045 | 1.699 | |
| 30 | 2.750 | 2.042 | 1.697 | K |
| 40 | 2.704 | 2.021 | 1.684 | |
| 60 | 2.660 | 2.000 | 1.671 | |
| 120 | 2.617 | 1.980 | 1.658 | Departme |
| 00 | 2.576 | 1.960 | 1.645 | Departme |













| | Question 1 | |
|--------------------------------------|--|---|
| ontractor has tl ard deviation, a | e following air void data from lot nd variance? | 8. What is the mean, |
| | | |
| Cont | actor | |
| Sublot | Air Voids | |
| | (%) | |
| 8A | 5.06 | |
| 8B | 4.73 | |
| 8C | 4.19 | |
| 8D | 3.64 | |
| 8E | 2.75 | |
| | | |
| | | Kansas Department of Transportation |

| | C | uestion 1 | |
|----------|---------------------------------|--------------------------|------------------------------|
| | ne following a and variance? | ir void data from lot 8. | What is the mean, |
| Cont | ractor | | |
| Sublot | Air Voids | | |
| | (%) | <i>n</i> = 5 | |
| 8A 8B | 5.06 4.73 | $\overline{X} = 4.07\%$ | |
| 8C 8D | 4.19 3.64 | S = 0.92% | |
| 8E | 2.75 | $S^2 = 0.85\%$ | |
| | | | Department of Transportation |

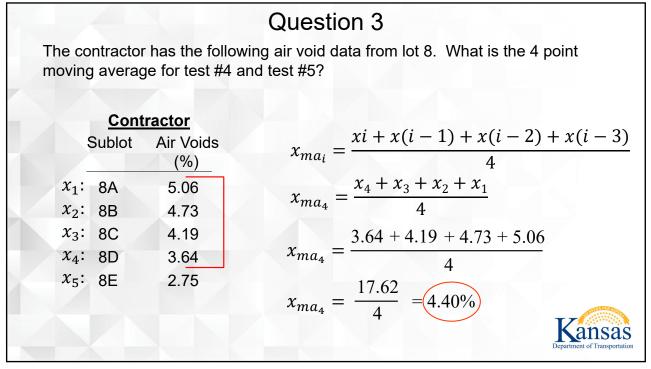
| (USL) is 5. | 25% and t | he Lower S | Spec Limit (LSL) i | m lot 8. The Upper Spec Limit is 2.75%. What is the Lower eent Within Limits? |
|-------------|----------------------|--|---|---|
| | Sublot 8A | r <u>actor</u> Air Voids (%) 5.06 | n = 5 $\overline{X} = 4.07\%$ S = 0.92% | $Q_u = \frac{(USL - \bar{X})}{s}$ $Q_L = \frac{(\bar{X} - LSL)}{s}$ |
| | 8B 8C 8D 8E | 4.73 4.19 3.64 2.75 | $S^2 = 0.85\%$ LSL = 2.75% | $PWL = (PWL_U + PWL_L) - 100$ |
| | | | USL = 5.25% | Kansas Department of Transportation |

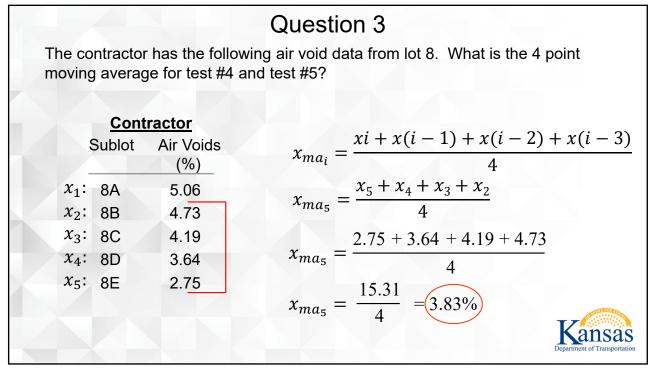
| The contractor has the followin (USL) is 5.25% and the Lower Quality Index, Upper Quality In | Spec Limit (LSL) is 2 | 2.75%. What is the Lower |
|---|---|---|
| Contractor Sublot Air Voids (%) 8A 5.06 8B 4.73 8C 4.19 8D 3.64 8E 2.75 | n = 5 $\overline{X} = 4.07\%$ S = 0.92% $S^2 = 0.85\%$ LSL = 2.75% USL = 5.25% | $Q_{u} = \frac{(5.25 - 4.07)}{0.92}$ $Q_{u} = \frac{(1.18)}{0.92} = 1.28$ $Q_{L} = \frac{(4.07 - 2.75)}{0.92}$ $Q_{L} = \frac{(1.32)}{0.92} = 1.43$ $E_{\text{L}} = \frac{(1.32)}{0.92} = 1.43$ |

| | | | | | Table | 2 for Es | | | | | imits | | | |
|--------------------|----------------|------------|-------|------------|------------|------------|------------|------------|-------------|-------------|-------------|-------------|-------------|--------------|
| | | | | | | | 5 | | n Proced | | | | | |
| | | | | | | St | andard | Deviatio | n Metho | d | | | | |
| | Quality | | | | | | | | | | | | | |
| | Index | | | | Pe | rcent Wit | hin Limi | ts for Se | lected Sa | mple Siz | es | | | |
| | Q_U or Q_L | <u>N=3</u> | N=4 | <u>N=5</u> | <u>N=6</u> | <u>N=7</u> | <u>N=8</u> | <u>N=9</u> | <u>N=10</u> | <u>N=15</u> | <u>N=20</u> | <u>N=30</u> | <u>N=50</u> | <u>N=100</u> |
| n=5 | | | | \square | | | | | | | | | | |
| | 1.18 | 100.00 | 89.33 | 88.71 | 88.53 | 88.44 | 88.39 | 88.35 | 88.32 | 88.25 | 88.21 | 88.18 | 88.15 | 88.12 |
| $Q_U = 1.28$ | 1.19 | 100.00 | 89.67 | 88.98 | 88.77 | 88.67 | 88.61 | 88.57 | 88.54 | 88.46 | 88.42 | 88.38 | 88.35 | 88.32 |
| | 1.20 | 100.00 | 90.00 | 89.24 | 89.01 | 88.90 | 88.83 | 88.79 | 88.76 | 88.66 | 88.62 | 88.58 | 88.54 | 88.52 |
| $PWL_{II} = 91.29$ | 1.21 | 100.00 | 90.33 | 89.50 | 89.25 | 89.13 | 89.06 | 89.00 | 88.97 | 88.87 | 88.82 | 88.78 | 88.74 | 88.71 |
| U | 1.22 | 100.00 | 90.67 | 89.77 | 89.49 | 89.35 | 89.27 | 89.22 | 89.18 | 89.07 | 89.02 | 88.97 | 88.93 | 88.91 |
| | 1.23 | 100.00 | 91.00 | 90.03 | 89.72 | 89.58 | 89.49 | 89.43 | 89.39 | 89.27 | 89.22 | 89.16 | 89.12 | 89.09 |
| | 1.24 | 100.00 | 91.33 | 90.28 | 89.96 | 89.80 | 89.70 | 89.64 | 89.59 | 89.47 | 89.41 | 89.36 | 89.31 | 89.28 |
| | 1.25 | 100.00 | 91.67 | 90.54 | 90.19 | 90.02 | 89.91 | 89.85 | 89.79 | 89.66 | 89.60 | 89.54 | 89.50 | 89.47 |
| | 1.26 | 100.00 | 92.00 | 90.79 | 90.42 | 90.23 | 90.12 | 90.05 | 90.00 | 89.85 | 89.79 | 89.73 | 89.68 | 89.65 |
| | 1.27 | 100.00 | 92.33 | 91.04 | 90.64 | 90.45 | 90.33 | 90.25 | 90.19 | 90.04 | 89.98 | 89.91 | 89.87 | 89.83 |
| | 1.28 | 100.00 | 92.67 | 91.29 | 90.87 | 90.66 | 90.53 | 90.45 | 90.39 | 90.23 | 90.16 | 90.10 | 90.05 | 90.01 |
| | 1.29 | 100.00 | 93.00 | 91.54 | 91.09 | 90.87 | 90.74 | 90.65 | 90.58 | 90.42 | 90.34 | 90.28 | 90.22 | 90.18 |
| | 1.30 | 100.00 | 93.33 | 91.79 | 91.31 | 91.07 | 90.94 | 90.84 | 90.78 | 90.60 | 90.52 | 90.45 | 90.40 | 90.36 |
| | 1.31 | 100.00 | 93.67 | 92.03 | 91.52 | 91.28 | 91.13 | 91.04 | 90.97 | 90.78 | 90.70 | 90.63 | 90.57 | 90.53 |
| | 1.32 | 100.00 | 94.00 | 92.27 | 91.74 | 91.48 | 91.33 | 91.23 | 91.15 | 90.96 | 90.88 | 90.80 | 90.74 | 90.70 |
| | 1.33 | 100.00 | 94.33 | 92.51 | 91.95 | 91.68 | 91.52 | 91.41 | 91.34 | 91.14 | 91.05 | 90.97 | 90.91 | 90.87 |
| | 1.34 | 100.00 | 94.67 | 92.75 | 92.16 | 91.88 | 91.71 | 91.60 | 91.52 | 91.31 | 91.22 | 91.14 | 91.08 | 91.03 |
| | | | | | | | | | | | | | | |

| | | | | | Table | | timation ability U andard 1 | Jnknown | n Proced | ure | imits | | | |
|-------------------|------------------|------------|------------|-------|------------|------------|-----------------------------------|------------|-------------|-------------|-------------|-------------|-------------|--------------|
| | Quality Index | | | | Per | cent Wit | hin Limi | ts for Sel | lected Sa | mple Siz | es | | | |
| n = 5 | Q_U or Q_L | <u>N=3</u> | <u>N=4</u> | N=5 | <u>N=6</u> | <u>N=7</u> | <u>N=8</u> | <u>N=9</u> | <u>N=10</u> | <u>N=15</u> | <u>N=20</u> | <u>N=30</u> | <u>N=50</u> | <u>N=100</u> |
| 0 1 1 2 | 1.35 | 100.00 | 95.00 | 92.98 | 92.37 | 92.08 | 91.90 | 91.78 | 91.70 | 91.48 | 91.39 | 91.31 | 91.24 | 91.19 |
| $Q_L = 1.43$ | 1.36 | 100.00 | 95.33 | 93.21 | 92.58 | 92.27 | 92.09 | 91.96 | 91.88 | 91.65 | 91.56 | 91.47 | 91.40 | 91.35 |
| | 1.37 | 100.00 | 95.67 | 93.44 | 92.78 | 92.46 | 92.27 | 92.14 | 92.05 | 91.82 | 91.72 | 91.63 | 91.56 | 91.51 |
| $PWL_{L} = 94.77$ | 1.38 | 100.00 | 96.00 | 93.67 | 92.98 | 92.65 | 92.45 | 92.32 | 92.23 | 91.99 | 91.88 | 91.79 | 91.72 | 91.67 |
| L | 1.39 | 100.00 | 96.33 | 93.90 | 93.18 | 92.83 | 92.63 | 92.49 | 92.40 | 92.15 | 92.04 | 91.95 | 91.88 | 91.82 |
| | 1.40 | 100.00 | 96.67 | 94.12 | 93.37 | 93.02 | 92.81 | 92.67 | 92.56 | 92.31 | 92.20 | 92.10 | 92.03 | 91.98 |
| | 1.41 | 100.00 | 97.00 | 94.34 | 93.57 | 93.20 | 92.98 | 92.83 | 92.73 | 92.47 | 92.36 | 92.26 | 92.18 | 92.13 |
| | 1.42 | 100.00 | 97.33 | 94.56 | 93.76 | 93.38 | 93.15 | 93.00 | 92.90 | 92.63 | 92.51 | 92.41 | 92.33 | 92.27 |
| | 1.43 | 100.00 | 97.67 | 94.77 | 93.95 | 93.55 | 93.32 | 93.17 | 93.06 | 92.78 | 92.66 | 92.56 | 92.48 | 92.42 |
| | 1.44 | 100.00 | 98.00 | 94.98 | 94.13 | 93.73 | 93.49 | 93.33 | 93.22 | 92.93 | 92.81 | 92.70 | 92.62 | 92.56 |
| | 1.45 | 100.00 | 98.33 | 95.19 | 94.32 | 93.90 | 93.65 | 93.49 | 93.37 | 93.08 | 92.96 | 92.85 | 92.76 | 92.70 |
| | 1.46 | 100.00 | 98.67 | 95.40 | 94.50 | 94.07 | 93.81 | 93.65 | 93.53 | 93.23 | 93.10 | 92.99 | 92.90 | 92.84 |
| | 1.47 | 100.00 | 99.00 | 95.61 | 94.67 | 94.23 | 93.97 | 93.80 | 93.68 | 93.37 | 93.25 | 93.13 | 93.04 | 92.98 |
| | 1.48 | 100.00 | 99.33 | 95.81 | 94.85 | 94.40 | 94.13 | 93.96 | 93.83 | 93.52 | 93.39 | 93.27 | 93.18 | 93.12 |
| | 1.49 | 100.00 | 99.67 | 96.01 | 95.02 | 94.56 | 94.29 | 94.11 | 93.98 | 93.66 | 93.52 | 93.40 | 93.31 | 93.25 |
| | 1.50 | 100.00 | 100.00 | 96.20 | 95.19 | 94.72 | 94.44 | 94.26 | 94.13 | 93.80 | 93.66 | 93.54 | 93.45 | 93.38 |
| | 1.51 | 100.00 | 100.00 | 96.39 | 95.36 | 94.87 | 94.59 | 94.40 | 94.27 | 93.94 | 93.80 | 93.67 | 93.58 | 93.51 |
| | 1.52 | 100.00 | 100.00 | 96.58 | 95.53 | 95.03 | 94.74 | 94.55 | 94.41 | 94.07 | 93.93 | 93.80 | 93.71 | 93.64 |
| | 1.53 | 100.00 | 100.00 | 96.77 | 95.69 | 95.18 | 94.88 | 94.69 | 94.55 | 94.20 | 94.06 | 93.93 | 93.83 | 93.76 |

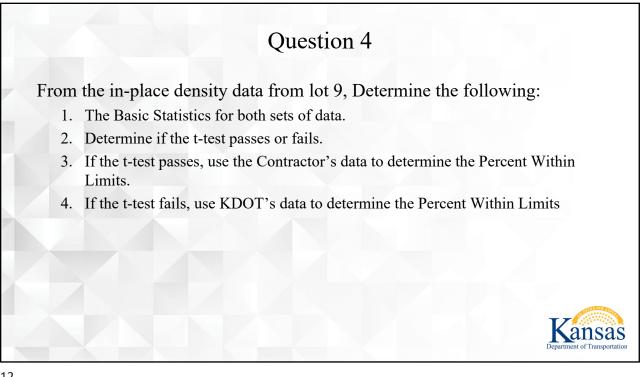
| 5.4L | | | Question 2 | |
|-------|------------|------------------|--|---|
| (USL) | is 5.25% a | and the Low | ving air void data fr er Spec Limit (LSL) | om lot 8. The Upper Spec Limit) is 2.75%. What is the Lower rcent Within Limits? |
| | Cont | ractor | n = 5 | $Q_u = 1.28$ |
| | Sublot | Air Voids (%) | X = 4.07% | $Q_L = 1.43$ |
| | 8A | 5.06 | S = 0.92% | $PWL = (PWL_U + PWL_L) - 100$ |
| | 8B 8C | 4.73 4.19 | $S^2 = 0.85\%$ | <i>PWL</i> = (91.29 + 94.77) - 100 |
| | 8D 8E | 3.64 2.75 | LSL = 2.75% | <i>PWL</i> = (186.06) - 100 |
| | OL | 2.15 | USL = 5.25% | <i>PWL</i> = 86.06 |
| | | | | Kansas Department of Transportation |



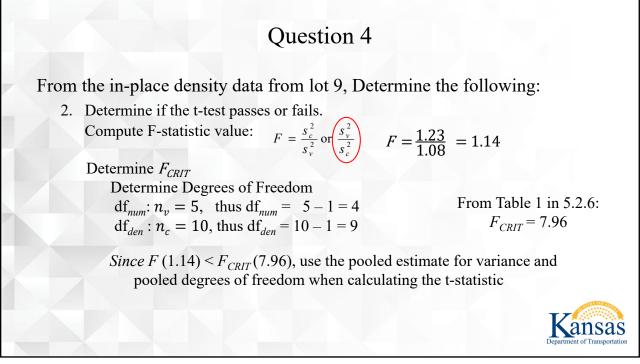


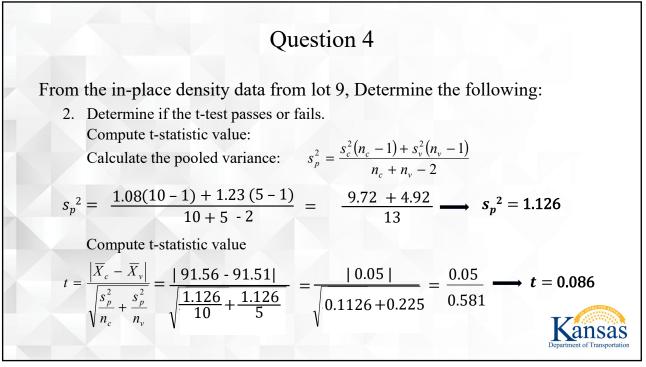
Question 4 The following in-place density data has been calculated from two different sets of test results from lot 9. The first set is from the contractor quality control tests and the second set of data is from KDOT verification tests. The Lower Specification Limit is 91.00%. Use a level of significance (a) = 1%.

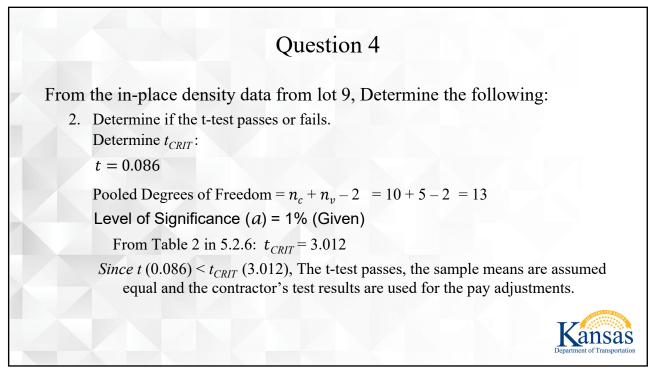
| Con | tractor | K | DOT | |
|--------|--------------------------------|--------|--------------------------------|--|
| Sublot | Density (%G _{mm}) | Sublot | Density (%G _{mm}) | |
| 9A1 | 92.10 | 9A | 91.84 | |
| 9A2 | 93.33 | 9B | 92.66 | |
| 9B1 | 90.72 | 9C | 91.87 | |
| 9B2 | 91.15 | 9D | 89.68 | |
| 9C1 | 92.27 | 9E | 91.49 | |
| 9C2 | 92.23 | | | |
| 9D1 | 89.51 | | | |
| 9D2 | 91.15 | | | STREET, ST |
| 9E1 | 91.84 | | | Kansas |
| 9E2 | 91.27 | | | Department of Transportation |

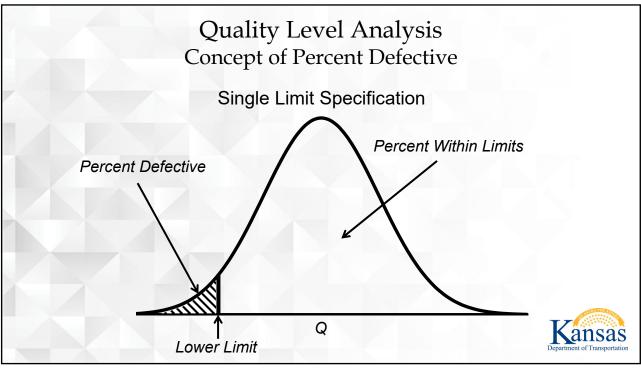


| | | Ques | stion 4 | | |
|--|--|---|--|----------------------------|---|
| 1. 1 | The Basic Sta | density data from a tistics for both sets of | | | U |
| <u>Co</u> Sublot | ntractor Density (%G _{mm}) | | | <u>r</u> Sublot | <u>XDOT</u> Density (%G _{mm}) |
| 9A1 9A2 9B1 9B2 9C1 9C2 | 92.10 93.33 90.72 91.15 92.27 92.23 | $n_c = 10$ $\bar{x}_c = 91.56$ $s_c = 1.04$ $s_c^2 = 1.08$ | $n_v = 5$ $\bar{x_v} = 91.51$ $s_v = 1.11$ $s_v^2 = 1.23$ | 9A 9B 9C 9D 9E | 91.84 92.66 91.87 89.68 91.49 |
| 9D1 9D2 9E1 9E2 | 89.51 91.15 91.84 91.27 | | | | Kar |









From the in-place density data from lot 9, Determine the following: 3. If the t-test passes, use the Contractor's data to determine the Percent Within Limits. Using the contractor's data we have: $\bar{x} = 91.56\%$ S = 1.04% n = 10 LSL = 91.00% (Given) $Q_L = \frac{(\bar{X} - LSL)}{S}$ $Q_L = \frac{(91.56 - 91.00)}{1.04} = \frac{(0.56)}{1.04} \longrightarrow Q_L = 0.54$ Enter Table 2 in 5.2.1 with $Q_L = 0.54$ and $n = 10 \longrightarrow PWL_L = 70.02\%$

Question 4

From the in-place density data from lot 9, Determine the following:

- 1. The Basic Statistics for both sets of data.
- 2. Determine if the t-test passes or fails.
- 3. If the t-test passes, use the Contractor's data to determine the Percent Within Limits.
- 4. If the t-test fails, use KDOT's data to determine the Percent Within Limits

